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**Honda et al.**

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(54) **AIR CONDITIONING APPARATUS**

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**ABSTRACT**

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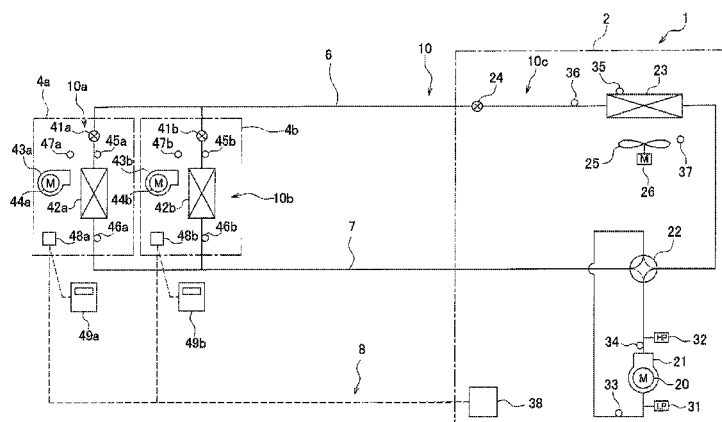
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An air conditioning apparatus has a refrigerant circuit made up of plural indoor units connected to an outdoor unit, and the air conditioning apparatus has a capacity controlling part and a target refrigerant temperature mode setting part. The capacity controlling part controls the air conditioning capacity of the outdoor unit in such a way that the evaporation temperature of refrigerant in the refrigerant circuit becomes a target evaporation temperature, or in such a way that the condensation temperature of the refrigerant becomes a target condensation temperature. The target refrigerant temperature mode setting part is configured to set a target refrigerant temperature mode to either a target refrigerant temperature changing mode or a target refrigerant temperature fixing mode. The target refrigerant temperature changing mode changes the target evaporation temperature or the target condensation temperature, and the target refrigerant temperature fixing mode fixes the target evaporation temperature or the target condensation temperature.

**21 Claims, 11 Drawing Sheets**



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*2700/21151* (2013.01); *F25B 2700/21152*  
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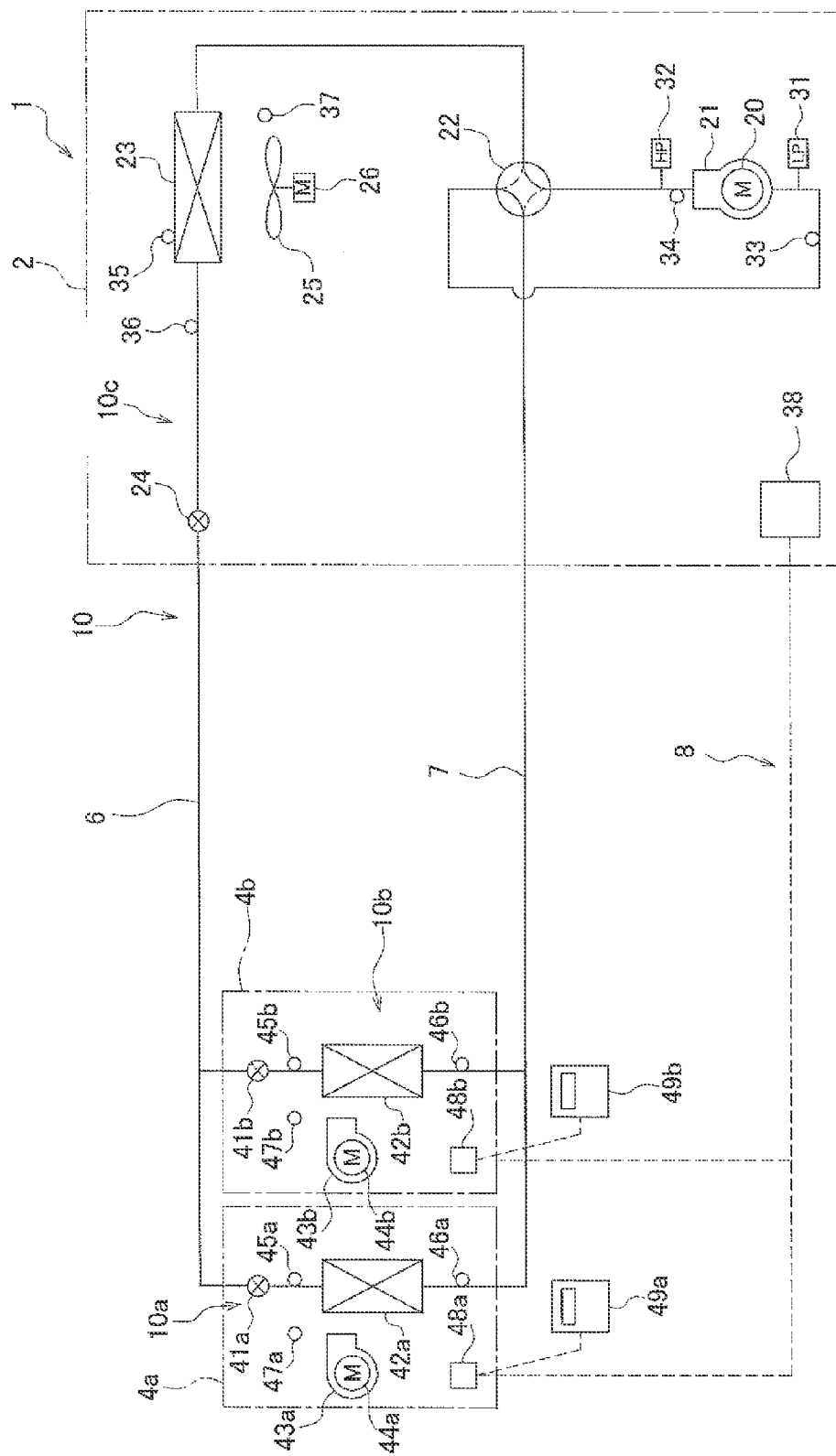


FIG. 1

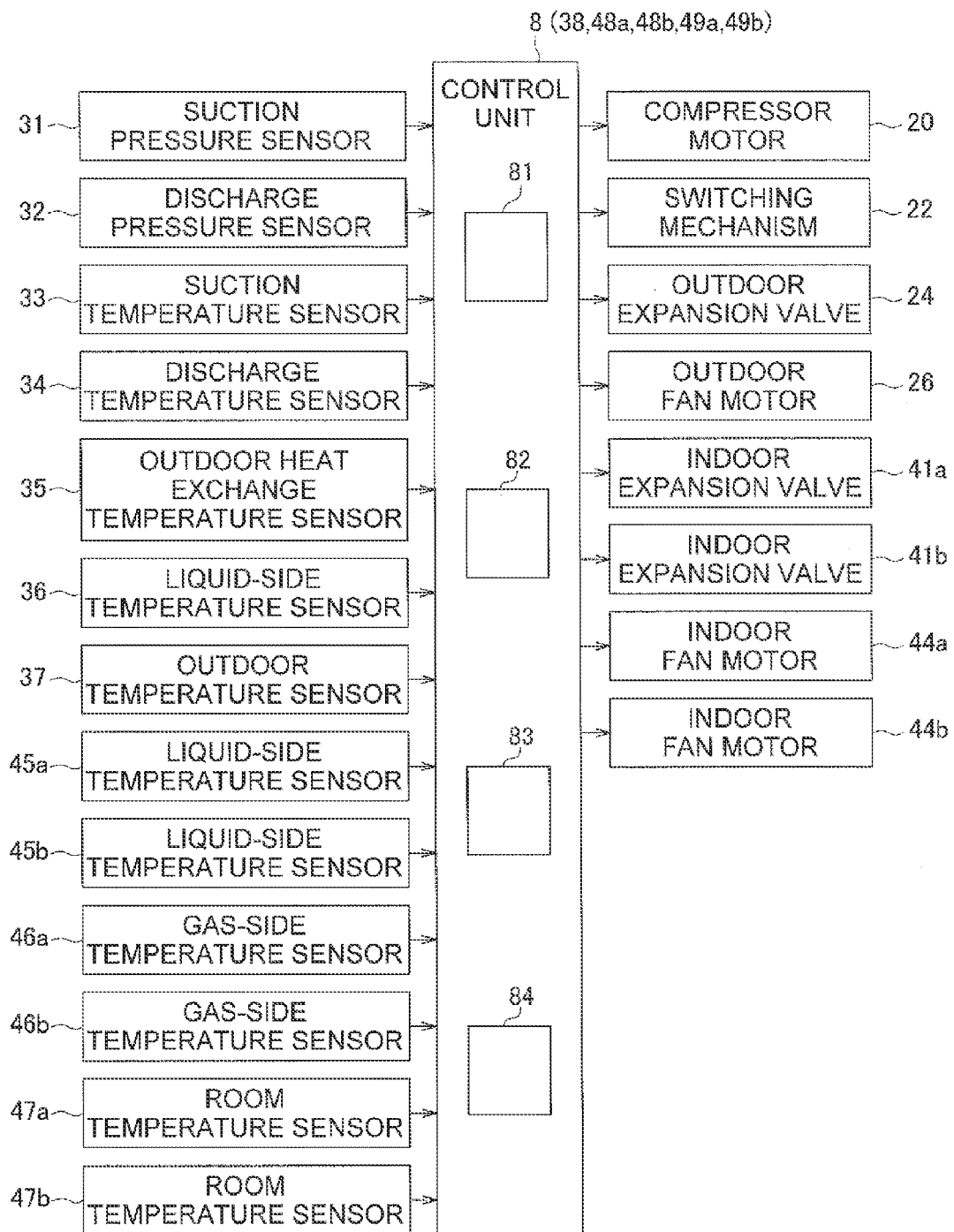


FIG. 2

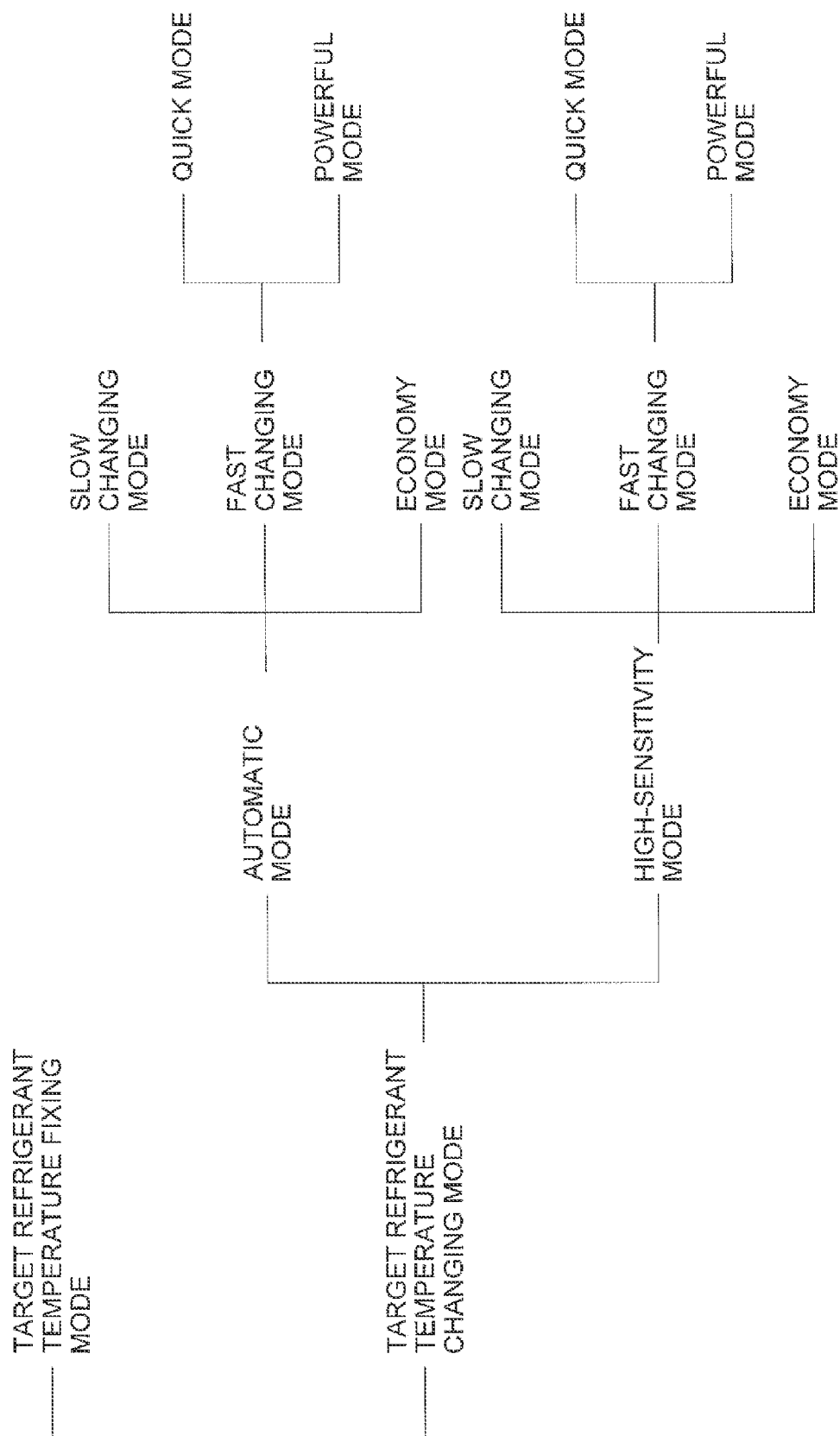


FIG. 3

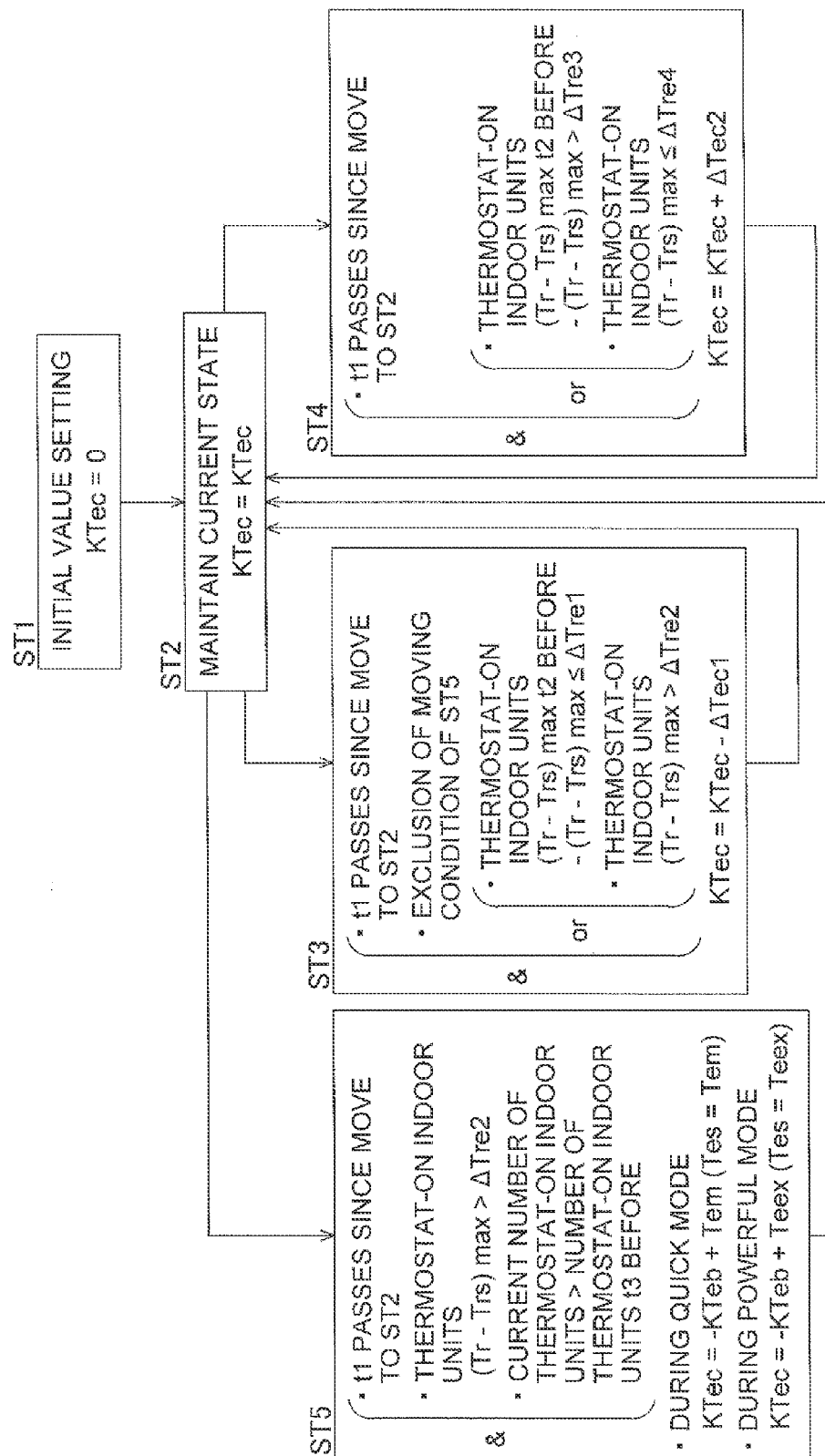


FIG. 4

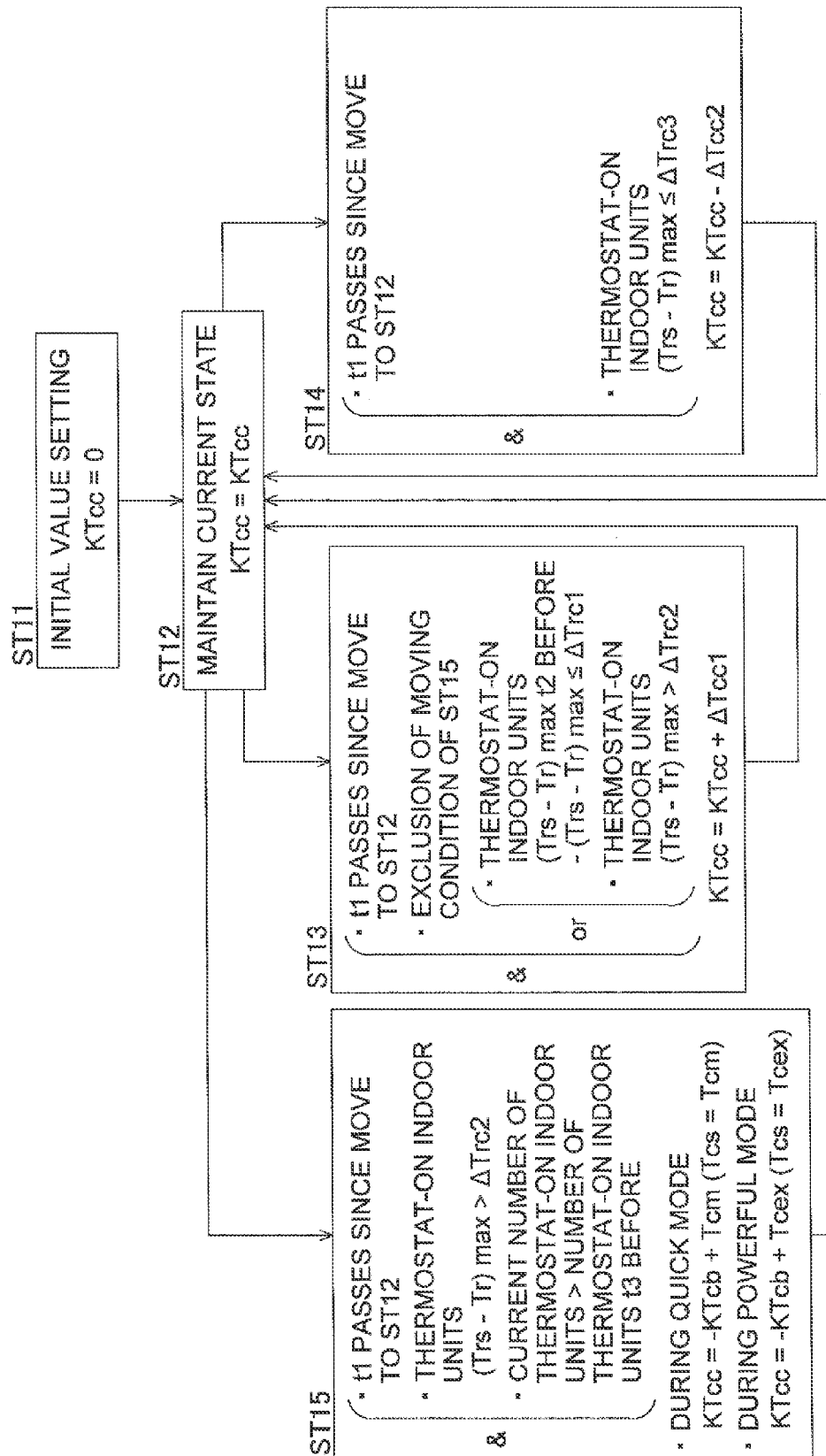


FIG. 5

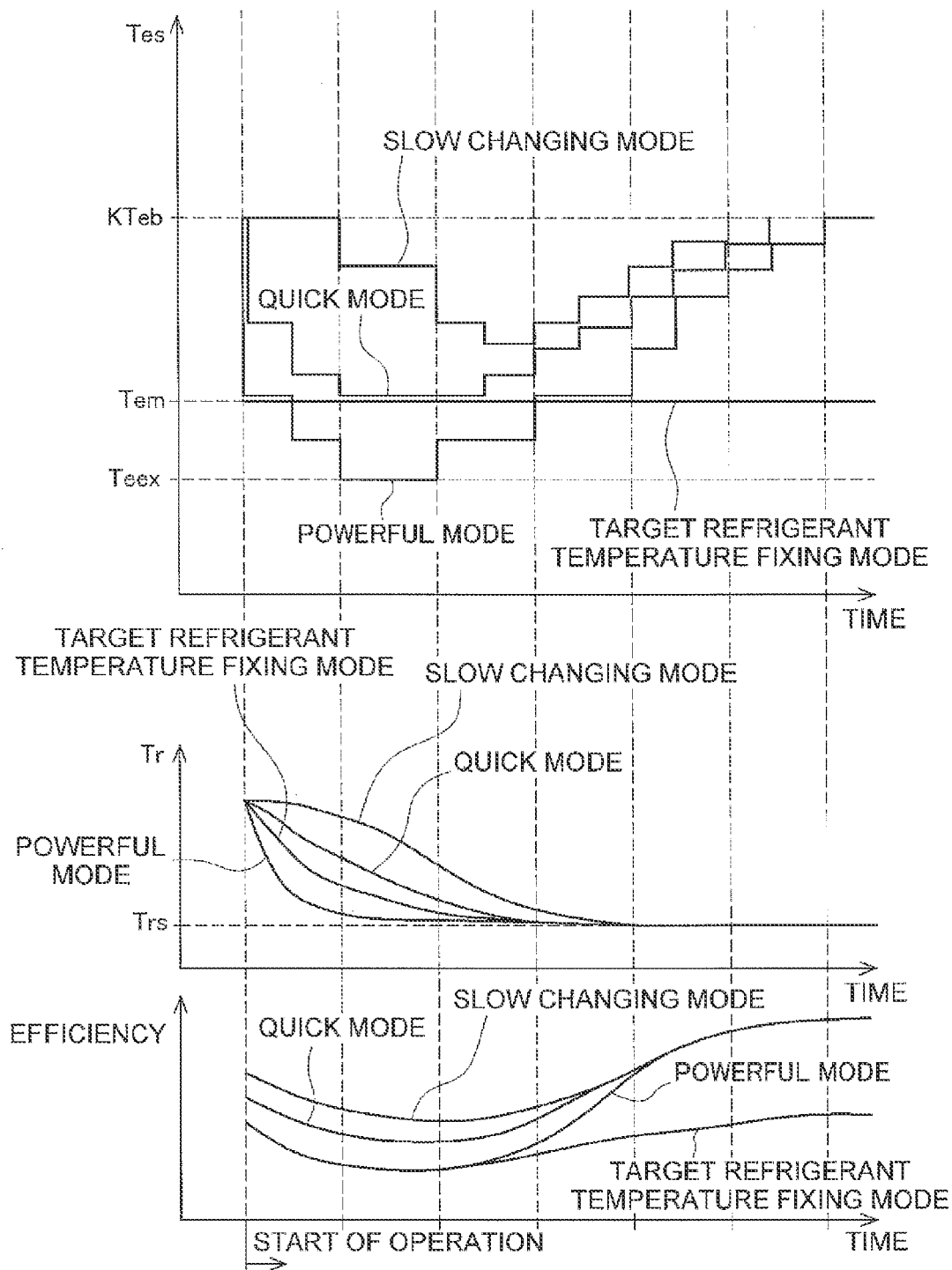


FIG. 6



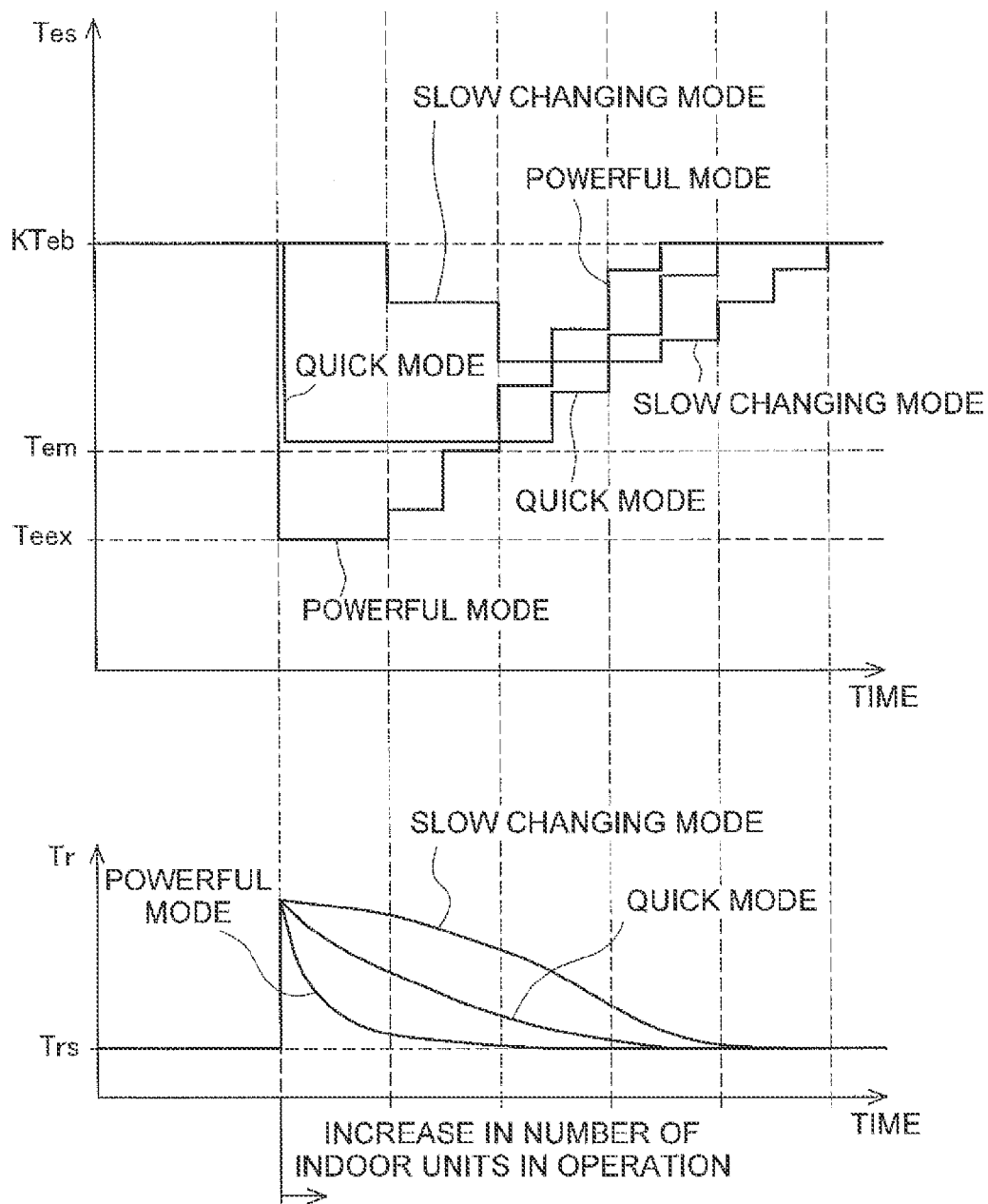


FIG. 7

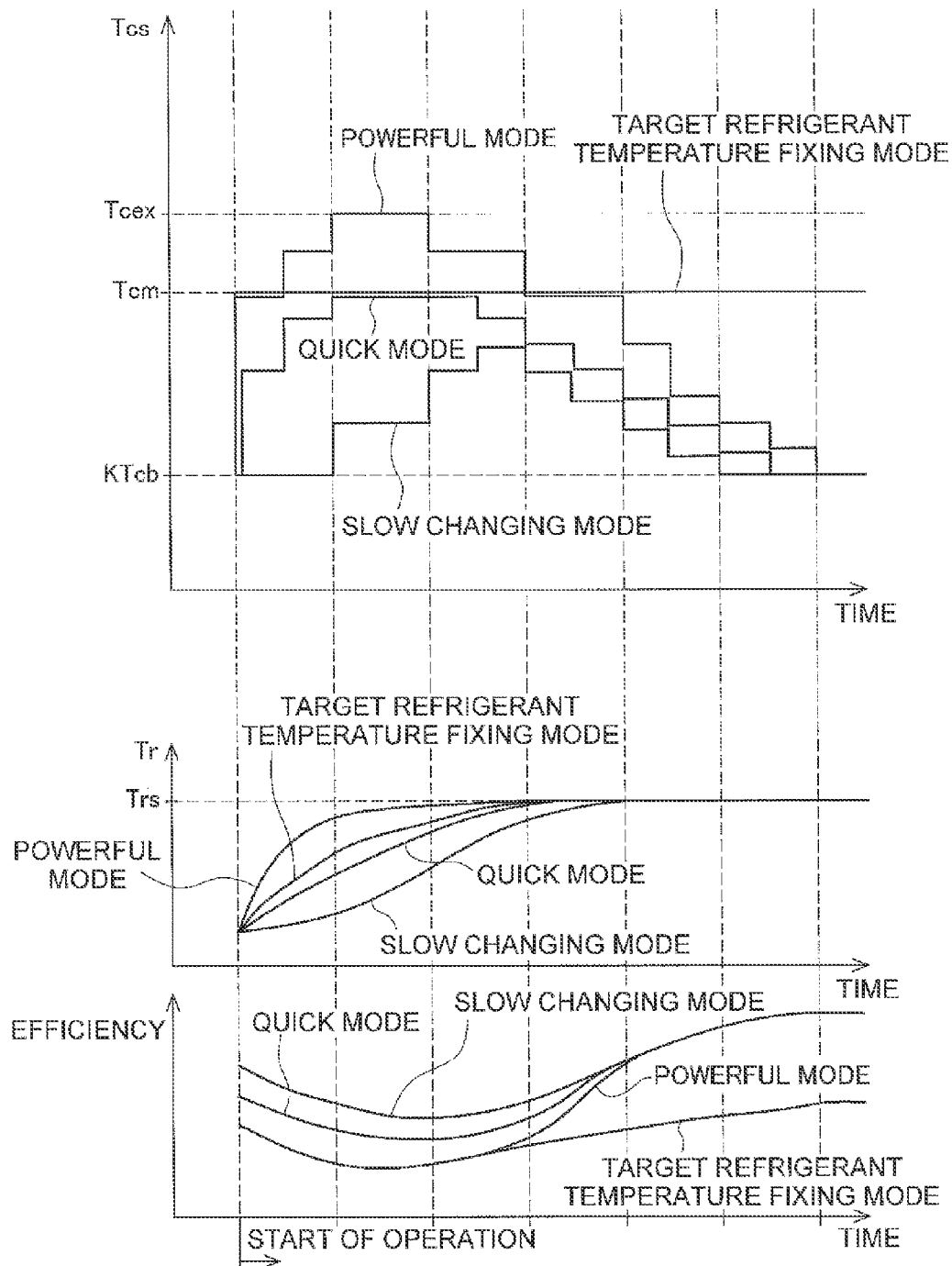


FIG. 8

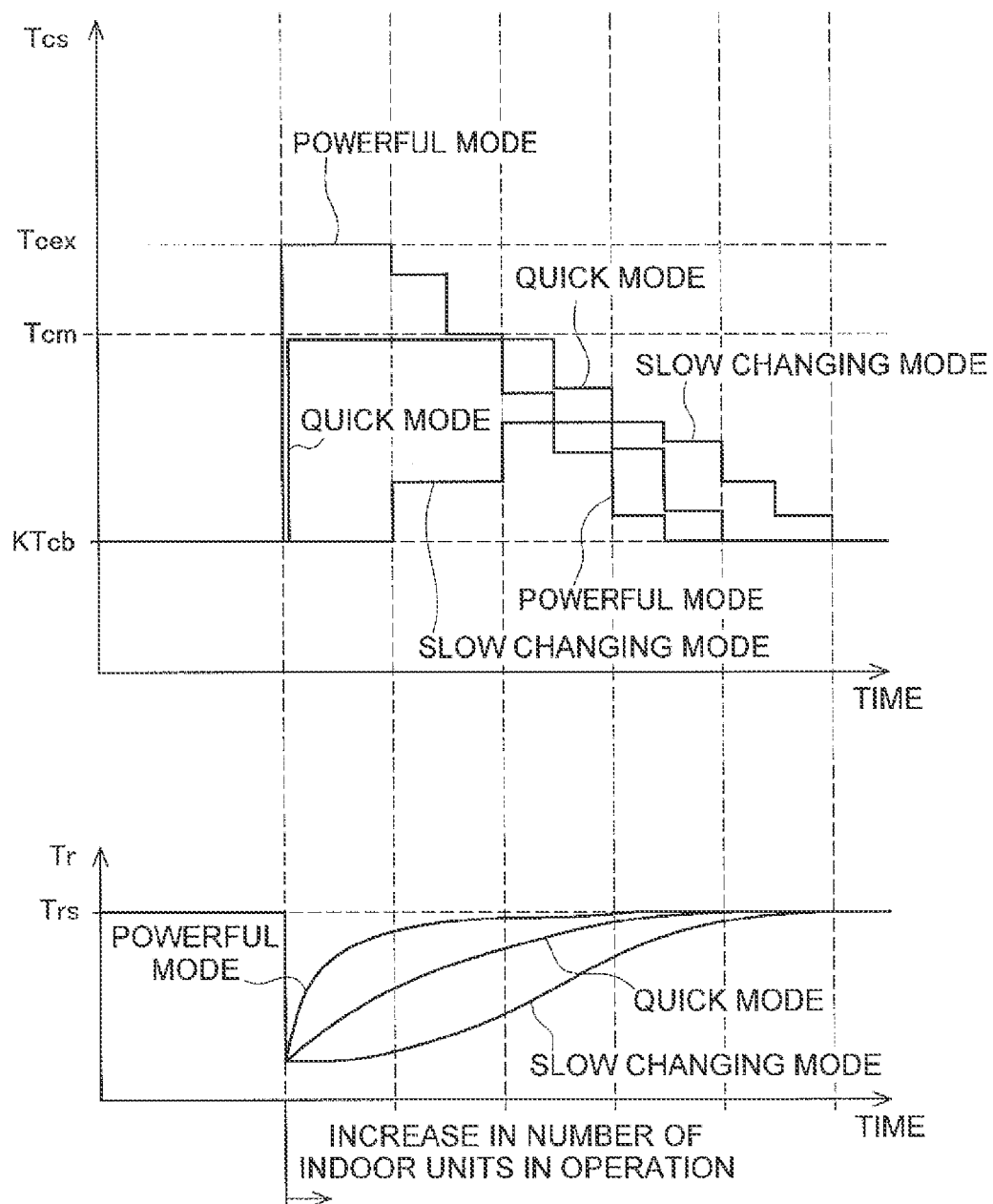


FIG. 9

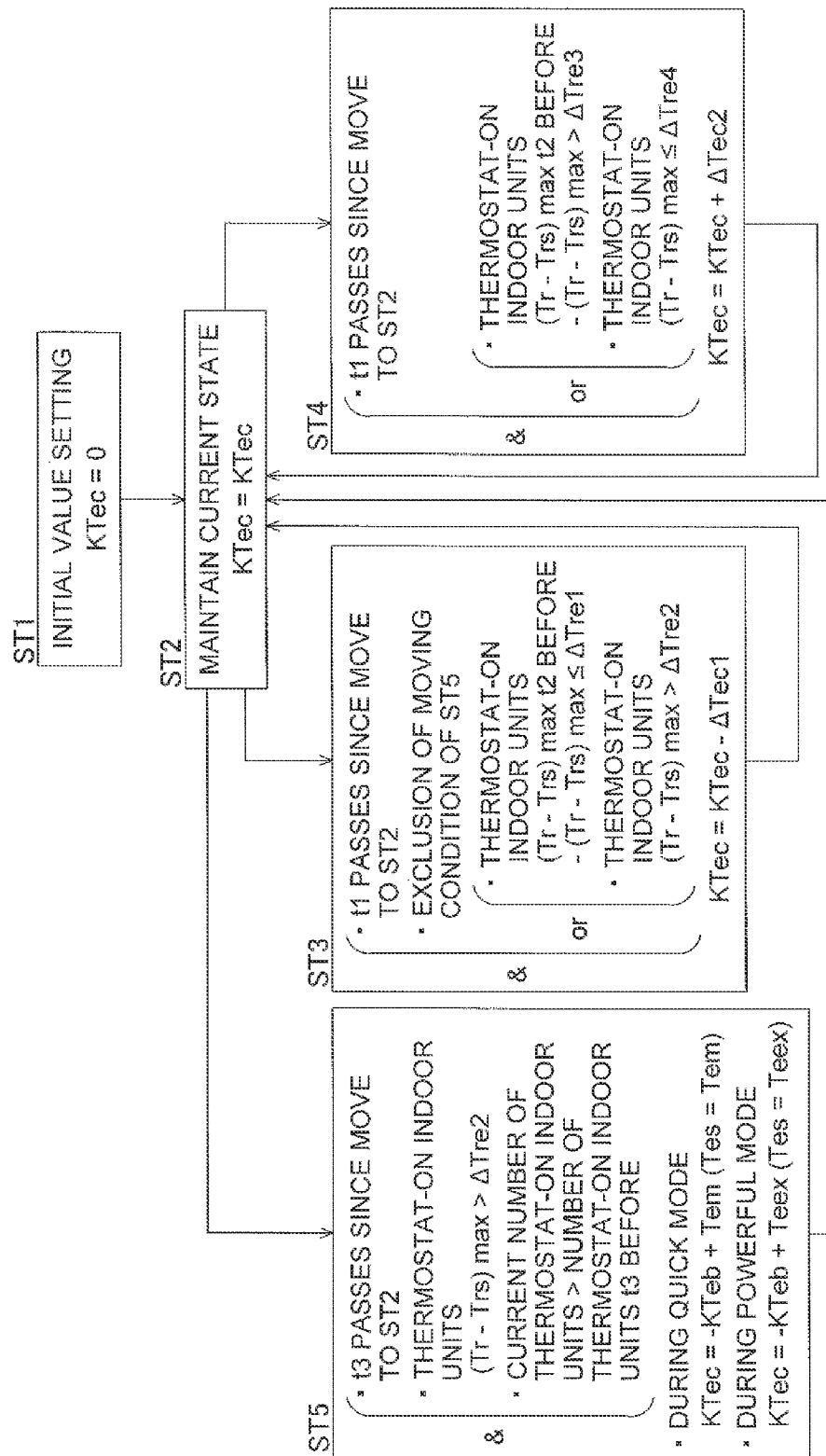


FIG. 10

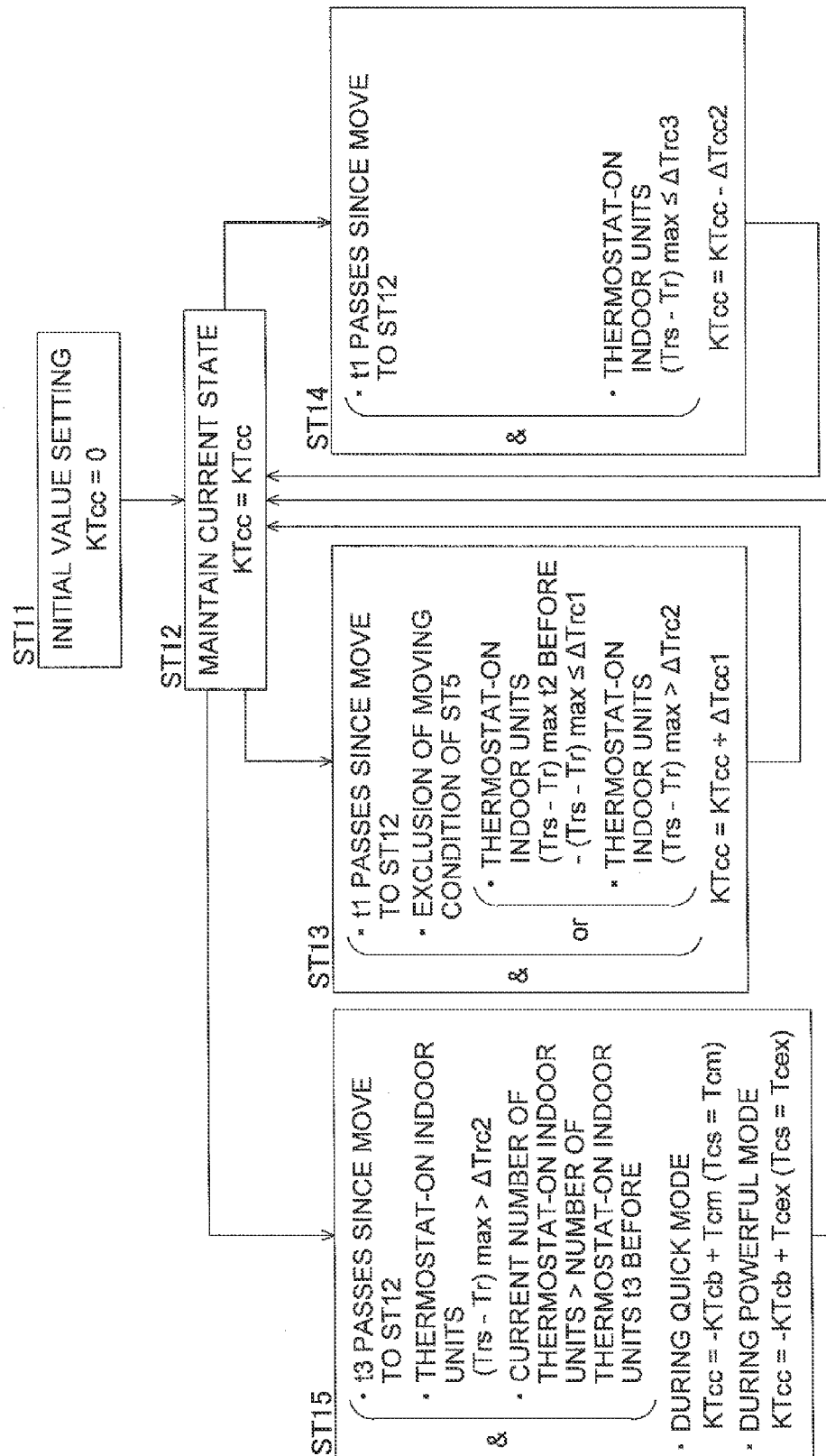


FIG. 11

## AIR CONDITIONING APPARATUS

## TECHNICAL FIELD

The present invention relates to an air conditioning apparatus and particularly an air conditioning apparatus equipped with a refrigerant circuit configured as a result of plural indoor units being connected to an outdoor unit.

## BACKGROUND ART

Conventionally, there has been an air conditioning apparatus equipped with a refrigerant circuit configured as a result of plural indoor units being connected to an outdoor unit. As this air conditioning apparatus, there is an air conditioning apparatus that has a capacity controlling part that controls the air conditioning capacity of the outdoor unit (specifically, the operating capacity of the compressor) in such a way that the evaporation temperature or the condensation temperature of refrigerant in the refrigerant circuit becomes a target evaporation temperature or a target condensation temperature. Additionally, as an example of an air conditioning apparatus that has a capacity controlling part, there is the air conditioning apparatus described in JP-A No. 2002-147823, which is configured in such a way as to change the target evaporation temperature or the target condensation temperature. Here, the target evaporation temperature or the target condensation temperature is changed in accordance with the air conditioning load characteristics of a building.

## SUMMARY

By changing the target evaporation temperature or the target condensation temperature as described above, an excess of the air conditioning capacity of the outdoor unit can be suppressed, the frequency with which the indoor units and the compressor alternate between being operated and being stopped can be reduced, and energy conservation can be improved. For this reason, the air conditioning apparatus easily satisfies users who prefer to conserve energy.

However, on the other hand, the amount of time it takes until the room temperatures of the air conditioned spaces reach set temperatures that are target values of the room temperatures tends to become longer in correspondence to the more the air conditioning capacity of the outdoor unit tends to be easily suppressed, and there is the concern that comfort will be compromised. For this reason, the air conditioning apparatus does not easily satisfy users who prefer comfort.

In this way, in the air conditioning apparatus, whether to give priority to energy conservation or whether to give priority to comfort differs depending on the preference of the user, so what is wanted is the provision of an air conditioning apparatus that can satisfy any user.

It is an object of the present invention to make it possible, in an air conditioning apparatus equipped with a refrigerant circuit configured as a result of plural indoor units being connected to an outdoor unit, for priority to be given to energy conservation or for priority to be given to comfort according to the preference of the user.

An air conditioning apparatus pertaining to a first aspect is an air conditioning apparatus equipped with a refrigerant circuit configured as a result of plural indoor units being connected to an outdoor unit, the air conditioning apparatus having a capacity controlling part and a target refrigerant temperature mode setting part. The capacity controlling part is a part that controls the air conditioning capacity of the outdoor unit in such a way that the evaporation temperature or

the condensation temperature of refrigerant in the refrigerant circuit becomes a target evaporation temperature or a target condensation temperature. The target refrigerant temperature mode setting part is a part for setting a target refrigerant temperature mode to either of a target refrigerant temperature changing mode that changes the target evaporation temperature or the target condensation temperature and a target refrigerant temperature fixing mode that fixes the target evaporation temperature or the target condensation temperature. Here, “evaporation temperature” means a state quantity that is equivalent to the evaporation pressure in the refrigerant circuit, and “condensation temperature” means a state quantity that is equivalent to the condensation pressure in the refrigerant circuit. That is, “evaporation pressure” and “evaporation temperature”, “target evaporation pressure” and “target evaporation temperature”, “condensation pressure” and “condensation temperature”, and “target condensation pressure” and “target condensation temperature” mean substantially the same state quantities even though the wordings themselves are different.

Here, the target refrigerant temperature mode can be set to either of the target refrigerant temperature changing mode and the target refrigerant temperature fixing mode by the target refrigerant temperature mode setting part. Additionally, when the target refrigerant temperature mode is set to the target refrigerant temperature changing mode, priority can be given to energy conservation, and when the target refrigerant temperature mode is set to the target refrigerant temperature fixing mode, priority can be given to comfort.

Because of this, here, priority can be given to energy conservation or priority can be given to comfort according to the preference of the user.

An air conditioning apparatus pertaining to a second aspect is the air conditioning apparatus pertaining to the first aspect, wherein the target refrigerant temperature changing mode has a fast changing mode and a slow changing mode. The fast changing mode is a mode that changes the target evaporation temperature or the target condensation temperature in such a way that room temperatures of air conditioned spaces targeted by the indoor units reach, in a short amount of time, set temperatures that are target values of the room temperatures. The slow changing mode is a mode that changes the target evaporation temperature or the target condensation temperature in such a way that the room temperatures reach the set temperatures in a longer amount of time than in the fast changing mode. Additionally, the fast changing mode and the slow changing mode are set by the target refrigerant temperature mode setting part.

Here, when the target refrigerant temperature mode is set to the target refrigerant temperature changing mode by the target refrigerant temperature mode setting part, the target refrigerant temperature mode can be set to either of two modes—the fast changing mode and the slow changing mode—in which the degree of control trackability is different. Additionally, when the target refrigerant temperature mode is set to the fast changing mode, control trackability is improved compared to a case where the target refrigerant temperature mode is set to the slow changing mode.

Because of this, here, by setting the target refrigerant temperature mode to the target refrigerant temperature changing mode, priority can be given to energy conservation, and at the same time the degree of control trackability can be changed according to the preference of the user.

An air conditioning apparatus pertaining to a third aspect is the air conditioning apparatus pertaining to the second aspect, wherein in the target refrigerant temperature fixing mode, the target evaporation temperature or the target condensation

temperature is fixed to a maximum capacity evaporation temperature or a maximum capacity condensation temperature corresponding to a case where the air conditioning capacity of the outdoor unit is at 100% capacity.

Here, the target evaporation temperature or the target condensation temperature is constantly fixed to the maximum capacity evaporation temperature or the maximum capacity condensation temperature.

Because of this, here, air conditioning operations can be performed in a state in which priority is constantly given to comfort.

An air conditioning apparatus pertaining to a fourth aspect is the air conditioning apparatus pertaining to the third aspect, wherein the fast changing mode has a powerful mode and a quick mode. The powerful mode is a mode that allows the target evaporation temperature or the target condensation temperature to be changed to a lowest evaporation temperature or a highest condensation temperature exceeding the maximum capacity evaporation temperature or the maximum capacity condensation temperature. The quick mode is a mode that does not allow the target evaporation temperature or the target condensation temperature to be changed to the lowest evaporation temperature or the highest condensation temperature. Additionally, the powerful mode and the quick mode are set by the target refrigerant temperature mode setting part.

Here, when the target refrigerant temperature mode is set to the fast changing mode of the target refrigerant temperature changing mode by the target refrigerant temperature mode setting part, the target refrigerant temperature mode can be set to either of two modes—the powerful mode and the quick mode—in which the degree of control trackability is further different. Additionally, when the target refrigerant temperature mode is set to the powerful mode, the target evaporation temperature or the target condensation temperature is allowed to be changed to the lowest evaporation temperature or the highest condensation temperature exceeding the maximum capacity evaporation temperature or the maximum capacity condensation temperature, so control trackability is further improved compared to a case where the target refrigerant temperature mode is set to the quick mode.

Because of this, here, by setting the target refrigerant temperature mode to the fast changing mode, control trackability can be improved, and at the same time the degree of control trackability can be further changed according to the preference of the user.

An air conditioning apparatus pertaining to a fifth aspect is the air conditioning apparatus pertaining to any of the second to fourth aspects, wherein the target refrigerant temperature changing mode further has an automatic mode and a high-sensitivity mode. The automatic mode is a mode that sets a reference target evaporation temperature or a reference target condensation temperature serving as a reference value of the target evaporation temperature or the target condensation temperature in accordance with an outdoor temperature of an outside space where the outdoor unit is disposed. The high-sensitivity mode is a mode in which a user sets the reference target evaporation temperature or the reference target condensation temperature. Additionally, the fast changing mode and the slow changing mode are set, together with the automatic mode or the high-sensitivity mode, by the target refrigerant temperature mode setting part. The target evaporation temperature or the target condensation temperature is changed by making, with respect to the reference target evaporation temperature or the reference target condensation temperature, a correction corresponding to the fast changing mode or the slow changing mode.

Here, when the target refrigerant temperature mode is set to the target refrigerant temperature changing mode by the target refrigerant temperature mode setting part, the target refrigerant temperature mode can be set to either of two modes—the automatic mode and the high-sensitivity mode—in which the way of setting the reference target evaporation temperature or the reference target condensation temperature is different. Additionally, when the target refrigerant temperature mode is set to the automatic mode, the reference target evaporation temperature or the reference target condensation temperature is set in accordance with the outdoor temperature, so the target evaporation temperature or the target condensation temperature that is set as a result of a correction corresponding to the fast changing mode and the slow changing mode being made to the reference target evaporation temperature or the reference target condensation temperature can further improve the degree of energy conservation compared to a case where the target refrigerant temperature mode is set to the high-sensitivity mode. On the other hand, when the target refrigerant temperature mode is set to the high-sensitivity mode, the degree of energy conservation can be set according to the preference of the user.

Because of this, here, by setting the target refrigerant temperature mode to the target refrigerant temperature changing mode, priority can be given to energy conservation, and at the same time the degree of energy conservation can be changed according to the preference of the user.

An air conditioning apparatus pertaining to a sixth aspect is the air conditioning apparatus pertaining to the fifth aspect, wherein the target refrigerant temperature changing mode further has an economy mode. The economy mode is a mode in which the reference target evaporation temperature or the reference target condensation temperature that has been set in the automatic mode or the high-sensitivity mode is set as the target evaporation temperature or the target condensation temperature without a correction being made to that reference target evaporation temperature or that reference target condensation temperature. Additionally, the economy mode is set, together with the automatic mode or the high-sensitivity mode, by the target refrigerant temperature mode setting part.

Here, when the target refrigerant temperature mode is set to the automatic mode or the high-sensitivity mode of the target refrigerant temperature changing mode by the target refrigerant temperature mode setting part, the target refrigerant temperature mode can be set to any of three modes including, in addition to the fast changing mode and the slow changing mode, the economy mode in which the way of correcting the reference target evaporation temperature or the reference target condensation temperature that has been set in the automatic mode or the high-sensitivity mode is different. Additionally, when the target refrigerant temperature mode is set to the economy mode, the target evaporation temperature or the target condensation temperature is set without a correction being made to the reference target evaporation temperature or the reference target condensation temperature, so the degree of control trackability can be brought closest to the preference of the user.

Because of this, here, by setting the target refrigerant temperature mode to the automatic mode or the high-sensitivity mode, the degree of energy conservation can be set, and at the same time the degree of control trackability can be changed according to the preference of the user.

An air conditioning apparatus pertaining to a seventh aspect is the air conditioning apparatus pertaining to the fifth or sixth aspect, wherein the reference target evaporation tem-

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perature is restricted to be equal to or less than an upper limit evaporation temperature that has been set in accordance with the room temperatures.

The reference target evaporation temperature is set in accordance with the outdoor temperature in the automatic mode and is set by the user in the high-sensitivity mode, so in an operating state in which the outdoor temperature is high and the room temperatures are low, there can be cases where the humidity in the air conditioned spaces becomes higher than the relative humidity (usually about 60%) suitable for the room temperatures. When the relative humidity becomes higher, discomfort increases in the air conditioned spaces, so this kind of operating state needs to be avoided.

Therefore, here, the reference target evaporation temperature that is set in the automatic mode and the high-sensitivity mode is restricted to be equal to or less than the upper limit evaporation temperature that has been set in accordance with the room temperatures, so it is ensured that the humidity in the air conditioned spaces becomes equal to or less than the relative humidity suitable for the room temperatures.

Because of this, here, discomfort in the air conditioned spaces can be suppressed, and at the same time the degree of energy conservation and the degree of control trackability can be changed according to the preference of the user.

#### BRIEF DESCRIPTION OF DRAWINGS

FIG. 1 is a schematic configuration diagram of an air conditioning apparatus pertaining to an embodiment of the present invention;

FIG. 2 is a control block diagram of the air conditioning apparatus;

FIG. 3 is a drawing showing various modes relating to a target evaporation temperature and a target condensation temperature that are settable;

FIG. 4 is a flowchart showing control for correcting the target evaporation temperature in a slow changing mode and a fast changing mode (a quick mode and a powerful mode);

FIG. 5 is a flowchart showing control for correcting the target condensation temperature in the slow changing mode and the fast changing mode (the quick mode and the powerful mode);

FIG. 6 is a drawing showing temporal changes, from the start of a cooling operation, in the target evaporation temperature, room temperatures, and efficiency in a target refrigerant temperature fixing mode and a target refrigerant temperature changing mode (the slow changing mode, the quick mode, and the powerful mode);

FIG. 7 is a drawing showing temporal changes in the target evaporation temperature and the room temperatures in the slow changing mode, the quick mode, and the powerful mode in a case where the number of indoor units in operation has increased during the cooling operation;

FIG. 8 is a drawing showing temporal changes, from the start of a heating operation, in the target condensation temperature, the room temperatures, and efficiency in the target refrigerant temperature fixing mode and the target refrigerant temperature changing mode (the slow changing mode, the quick mode, and the powerful mode);

FIG. 9 is a drawing showing temporal changes in the target condensation temperature and the room temperatures in the slow changing mode, the quick mode, and the powerful mode in a case where the number of indoor units in operation has increased during the heating operation;

FIG. 10 is a flowchart showing control for correcting the target evaporation temperature in the slow changing mode

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and the fast changing mode (the quick mode and the powerful mode) in example modification 1; and

FIG. 11 is a flowchart showing control for correcting the target condensation temperature in the slow changing mode and the fast changing mode (the quick mode and the powerful mode) in example modification 1.

#### DESCRIPTION OF EMBODIMENT

An embodiment of an air conditioning apparatus pertaining to the present invention will be described below on the basis of the drawings. The specific configurations of the embodiment of the air conditioning apparatus pertaining to the present invention are not limited to the following embodiment and its example modifications and can be changed without departing from the spirit of the invention.

##### (1) Basic Configuration of Air Conditioning Apparatus

FIG. 1 is a schematic configuration diagram of an air conditioning apparatus 1 pertaining to an embodiment of the present invention. The air conditioning apparatus 1 is an apparatus used to air condition the inside of a building or the like by performing a vapor compression refrigeration cycle operation. The air conditioning apparatus 1 is mainly configured as a result of an outdoor unit 2 and plural (here, two) indoor units 4a and 4b being connected to one another. Here, the outdoor unit 2 and the plural indoor units 4a and 4b are connected to one another via a liquid refrigerant connection pipe 6 and a gas refrigerant connection pipe 7. That is, a vapor compression refrigerant circuit 10 of the air conditioning apparatus 1 is configured as a result of the outdoor unit 2 and the plural indoor units 4a and 4b being connected to one another via the refrigerant connection pipes 6 and 7.

##### <Indoor Units>

The indoor units 4a and 4b are installed indoors. The indoor units 4a and 4b are connected to the outdoor unit 2 via the refrigerant connection pipes 6 and 7 and configure part of the refrigerant circuit 10.

Next, the configuration of the indoor units 4a and 4b will be described. The indoor unit 4b has the same configuration as the indoor unit 4a, so here just the configuration of the indoor unit 4a will be described; regarding the configuration of the indoor unit 4b, the letter "b" will be added instead of the letter "a" indicating each part of the indoor unit 4a, and description of each part of the indoor unit 4b will be omitted.

The indoor unit 4a mainly has an indoor-side refrigerant circuit 10a (an indoor-side refrigerant circuit 10b in the indoor unit 4b) that configures part of the refrigerant circuit 10. The indoor-side refrigerant circuit 10a mainly has an indoor expansion valve 41a and an indoor heat exchanger 42a.

The indoor expansion valve 41a is a valve that reduces the pressure of refrigerant flowing through the indoor-side refrigerant circuit 10a to thereby adjust the flow rate of the refrigerant. The indoor expansion valve 41a is an electrically powered expansion valve connected to the liquid side of the indoor heat exchanger 42a.

The indoor heat exchanger 42a comprises a cross-fin type fin and tube heat exchanger, for example. In the neighborhood of the indoor heat exchanger 42a, there is disposed an indoor fan 43a for delivering room air to the indoor heat exchanger 42a. Heat exchange takes place between the refrigerant and the room air in the indoor heat exchanger 42a as a result of the indoor fan 43a delivering the room air to the indoor heat exchanger 42a. The indoor fan 43a is driven to rotate by an



indoor fan motor **44a**. Because of this, the indoor heat exchanger **42a** functions as a radiator of the refrigerant and an evaporator of the refrigerant.

Furthermore, various sensors are disposed in the indoor unit **4a**. On the liquid side of the indoor heat exchanger **42a**, there is disposed a liquid-side temperature sensor **45a** that detects a temperature  $T_{rla}$  of the refrigerant in a liquid state or a gas-liquid two-phase state. On the gas side of the indoor heat exchanger **42a**, there is disposed a gas-side temperature sensor **46a** that detects a temperature  $T_{rga}$  of the refrigerant in a gas state. On the room air inlet side of the indoor unit **4a**, there is disposed a room temperature sensor **47a** that detects the temperature of the room air (i.e., a room temperature  $T_{ra}$ ) in the air conditioned space targeted by the indoor unit **4a**. Furthermore, the indoor unit **4a** has an indoor-side control unit **48a** that controls the actions of each part configuring the indoor unit **4a**. Additionally, the indoor-side control unit **48a** has a microcomputer, which is disposed in order to control the indoor unit **4a**, and a memory and the like, and the indoor-side control unit **48a** can exchange control signals and so forth with a remote controller **49a** for individually operating the indoor unit **4a** and can exchange control signals and so forth with the outdoor unit **2**. The remote controller **49a** is a device for a user to make various settings relating to air conditioning operations and issue operate/stop commands.

<Outdoor Unit>

The outdoor unit **2** is installed outdoors. The outdoor unit **2** is connected to the indoor units **4a** and **4b** via the refrigerant connection pipes **6** and **7** and configures part of the refrigerant circuit **10**.

Next, the configuration of the outdoor unit **2** will be described.

The outdoor unit **2** mainly has an outdoor-side refrigerant circuit **10c** that configures part of the refrigerant circuit **10**. The outdoor-side refrigerant circuit **10c** mainly has a compressor **21**, a switching mechanism **22**, an outdoor heat exchanger **23**, and an outdoor expansion valve **24**.

The compressor **21** is a closed compressor having a casing inside of which are housed a non-illustrated compression element and a compressor motor **20** that drives the compression element to rotate. The compressor motor **20** is supplied with electrical power via a non-illustrated inverter device, and its operating capacity can be changed by changing the frequency (i.e., the rotational speed) of the inverter device.

The switching mechanism **22** is a four-way switching valve for switching the direction of the flow of the refrigerant. During a cooling operation, which is one of the air conditioning operations, the switching mechanism **22** can interconnect the discharge side of the compressor **21** and the gas side of the outdoor heat exchanger **23** and also interconnect the suction side of the compressor **21** and the gas refrigerant connection pipe **7** in order to cause the outdoor heat exchanger **23** to function as a radiator of the refrigerant that has been compressed in the compressor **21** and cause the indoor heat exchangers **42a** and **42b** to function as evaporators of the refrigerant that has radiated heat in the outdoor heat exchanger **23** (a radiation switching state; see the solid lines of the switching mechanism **22** in FIG. 1), and during a heating operation, which is one of the air conditioning operations, the switching mechanism **22** can interconnect the discharge side of the compressor **21** and the gas refrigerant connection pipe **7** and also interconnect the suction side of the compressor **21** and the gas side of the outdoor heat exchanger **23** in order to cause the indoor heat exchangers **42a** and **42b** to function as radiators of the refrigerant that has been compressed in the compressor **21** and cause the outdoor heat exchanger **23** to function as an evaporator of the refrigerant

that has radiated heat in the indoor heat exchangers **42a** and **42b** (an evaporation switching state; see the dashed lines of the switching mechanism **22** in FIG. 1). The switching mechanism **22** does not have to be a four-way switching valve and may also be a mechanism configured by combining a three-way valve and an electromagnetic valve and the like to fulfill the same functions.

The outdoor heat exchanger **23** comprises a cross-fin type fin and tube heat exchanger, for example. In the neighborhood of the outdoor heat exchanger **23**, there is disposed an outdoor fan **25** for delivering outdoor air to the outdoor heat exchanger **23**. Heat exchange takes place between the refrigerant and the outdoor air in the outdoor heat exchanger **23** as a result of the outdoor fan **25** delivering the outdoor air to the outdoor heat exchanger **23**. The outdoor fan **25** is driven to rotate by an outdoor fan motor **26**. Because of this, the outdoor heat exchanger **23** functions as a radiator of the refrigerant and an evaporator of the refrigerant.

The outdoor expansion valve **24** is a valve that reduces the pressure of the refrigerant flowing through the outdoor-side refrigerant circuit **10c**. The outdoor expansion valve **24** is an electrically powered expansion valve connected to the liquid side of the outdoor heat exchanger **23**.

Furthermore, various sensors are disposed in the outdoor unit **2**. In the outdoor unit **2**, there are disposed a suction pressure sensor **31** that detects a suction pressure  $P_s$  of the compressor **21**, a discharge pressure sensor **32** that detects a discharge pressure  $P_d$  of the compressor **21**, a suction temperature sensor **33** that detects a suction temperature  $T_s$  of the compressor **21**, and a discharge temperature sensor **34** that detects a discharge temperature  $T_d$  of the compressor **21**. In the outdoor heat exchanger **23**, there is disposed an outdoor heat exchange temperature sensor **35** that detects a temperature  $T_{ol1}$  of the refrigerant in a gas-liquid two-phase state. On the liquid side of the outdoor heat exchanger **23**, there is disposed a liquid-side temperature sensor **36** that detects a temperature  $T_{ol2}$  of the refrigerant in a liquid state or a gas-liquid two-phase state. On the outdoor air inlet side of the outdoor unit **2**, there is disposed an outdoor temperature sensor **37** that detects the temperature of the outdoor air (i.e., an outdoor temperature  $T_a$ ) in the outside space where the outdoor unit **2** is disposed. Furthermore, the outdoor unit **2** has an outdoor-side control unit **38** that controls the actions of each part configuring the outdoor unit **2**. Additionally, the outdoor-side control unit **38** has a microcomputer, which is disposed in order to control the outdoor unit **2**, a memory, and an inverter device and the like that controls the compressor motor **20**, and the outdoor-side control unit **38** can exchange control signals and so forth with the indoor-side control units **48a** and **48b** of the indoor units **4a** and **4b**.

<Refrigerant Connection Pipes>

The refrigerant connection pipes **6** and **7** are refrigerant pipes installed on site when installing the air conditioning apparatus **1**, and pipes having various lengths and pipe diameters depending on the installation conditions of the outdoor unit **2** and the indoor units **4a** and **4b** are used.

<Control Unit>

As shown in FIG. 1, the remote controllers **49a** and **49b** for individually operating the indoor units **4a** and **4b**, the indoor-side control units **48a** and **48b** of the indoor units **4a** and **4b**, and the outdoor-side control unit **38** of the outdoor unit **2** configure a control unit **8** that controls the operations of the entire air conditioning apparatus **1**. As shown in FIG. 2, the control unit **8** is connected in such a way that it can receive detection signals of the various sensors **31** to **37**, **45a**, **45b**, **46a**, **46b**, **47a**, and **47b** and so forth. Additionally, the control unit **8** is configured in such a way that it can perform the air

conditioning operations (the cooling operation and the heating operation) by controlling the various devices and valves 20, 22, 24, 26, 41a, 41b, 44a, and 44b on the basis of these detection signals and so forth. Furthermore, here, the control unit 8 mainly has a capacity controlling part 81, an indoor controlling part 82, a target refrigerant temperature mode setting part 83, and a target refrigerant temperature changing part 84. The capacity controlling part 81 is a part that controls the air conditioning capacity of the outdoor unit 2 in such a way that an evaporation temperature  $T_e$  or a condensation temperature  $T_c$  of the refrigerant in the refrigerant circuit 10 becomes a target evaporation temperature  $T_{es}$  or a target condensation temperature  $T_{cs}$ . The indoor controlling part 82 is a part that controls the devices and valves 41a, 41b, 44a, and 44b of the indoor units 4a and 4b in such a way that the room temperatures  $T_{ra}$  and  $T_{rb}$  of the air conditioned spaces targeted by the indoor units 4a and 4b become set temperatures  $T_{ras}$  and  $T_{rbs}$  that are target values of the room temperatures  $T_{ra}$  and  $T_{rb}$ . The target refrigerant temperature mode setting part 83 is a part for setting modes relating to the target evaporation temperature  $T_{es}$  and the target condensation temperature  $T_{cs}$ , such as setting whether to change or fix the target evaporation temperature  $T_{es}$  or the target condensation temperature  $T_{cs}$ . The target refrigerant temperature changing part 84 is a part for changing or fixing the target evaporation temperature  $T_{es}$  and the target condensation temperature  $T_{cs}$  in accordance with the mode that has been set by the target refrigerant temperature mode setting part 83. Here, FIG. 2 is a control block diagram of the air conditioning apparatus 1.

As described above, the air conditioning apparatus 1 has the refrigerant circuit 10 that is configured as a result of the plural (here, two) indoor units 4a and 4b being connected to the outdoor unit 2. Additionally, in the air conditioning apparatus 1, the following air conditioning operations and control

## (2) Basic Actions of Air Conditioning Apparatus

Next, the basic actions of the air conditioning operations (the cooling operation and the heating operation) of the air conditioning apparatus 1 will be described using FIG. 1.

### <Cooling Operation>

When a cooling operation command is given from the remote controllers 49a and 49b, the switching mechanism 22 is switched to a radiation operating state (the state indicated by the solid lines of the switching mechanism 22 in FIG. 1), and the compressor 21, the outdoor fan 25, and the indoor fans 43a and 43b start up.

Then, the low-pressure gas refrigerant in the refrigerant circuit 10 is sucked into the compressor 21, is compressed, and becomes high-pressure gas refrigerant. The high-pressure gas refrigerant is sent via the switching mechanism 22 to the outdoor heat exchanger 23. The high-pressure gas refrigerant that has been sent to the outdoor heat exchanger 23 condenses and becomes high-pressure liquid refrigerant as a result of exchanging heat with the outdoor air supplied by the outdoor fan 25 and being cooled in the outdoor heat exchanger 23 functioning as a radiator of the refrigerant. The high-pressure liquid refrigerant is sent via the outdoor expansion valve 24 and the liquid refrigerant connection pipe 6 from the outdoor unit 2 to the indoor units 4a and 4b.

The high-pressure liquid refrigerant that has been sent to the indoor units 4a and 4b has its pressure reduced by the indoor expansion valves 41a and 41b and becomes low-pressure refrigerant in a gas-liquid two-phase state. The low-pressure refrigerant in the gas-liquid two-phase state is sent to

the indoor heat exchangers 42a and 42b. The low-pressure refrigerant in the gas-liquid two-phase state that has been sent to the indoor heat exchangers 42a and 42b evaporates and becomes low-pressure gas refrigerant as a result of exchanging heat with the room air supplied by the indoor fans 43a and 43b and being heated in the indoor heat exchangers 42a and 42b functioning as evaporators of the refrigerant. The low-pressure gas refrigerant is sent via the gas refrigerant connection pipe 7 from the indoor units 4a and 4b to the outdoor unit 2.

The low-pressure gas refrigerant that has been sent to the outdoor unit 2 is sucked via the switching mechanism 22 back into the compressor 21.

### <Heating Operation>

When a heating operation command is given from the remote controllers 49a and 49b, the switching mechanism 22 is switched to an evaporation operating state (the state indicated by the dashed lines of the switching mechanism 22 in FIG. 1), and the compressor 21, the outdoor fan 25, and the indoor fans 43a and 43b start up.

Then, the low-pressure gas refrigerant in the refrigerant circuit 10 is sucked into the compressor 21, is compressed, and becomes high-pressure gas refrigerant. The high-pressure gas refrigerant is sent via the switching mechanism 22 and the gas refrigerant connection pipe 7 from the outdoor unit 2 to the indoor units 4a and 4b.

The high-pressure gas refrigerant that has been sent to the indoor units 4a and 4b is sent to the indoor heat exchangers 42a and 42b. The high-pressure gas refrigerant that has been sent to the indoor heat exchangers 42a and 42b condenses and becomes high-pressure liquid refrigerant as a result of exchanging heat with the room air supplied by the indoor fans 43a and 43b and being cooled in the indoor heat exchangers 42a and 42b functioning as radiators of the refrigerant. The high-pressure liquid refrigerant has its pressure reduced by the indoor expansion valves 41a and 41b. The refrigerant whose pressure has been reduced by the indoor expansion valves 41a and 41b is sent via the liquid refrigerant connection pipe 6 from the indoor units 4a and 4b to the outdoor unit 2.

The refrigerant that has been sent to the outdoor unit 2 is sent to the outdoor expansion valve 24, has its pressure reduced by the outdoor expansion valve 24, and becomes low-pressure refrigerant in a gas-liquid two-phase state. The low-pressure refrigerant in the gas-liquid two-phase state is sent to the outdoor heat exchanger 23. The low-pressure refrigerant in the gas-liquid two-phase state that has been sent to the outdoor heat exchanger 23 evaporates and becomes low-pressure gas refrigerant as a result of exchanging heat with the outdoor air supplied by the outdoor fan 25 and being heated in the outdoor heat exchanger 23 functioning as an evaporator of the refrigerant. The low-pressure gas refrigerant is sucked via the switching mechanism 22 back into the compressor 21.

### <Basic Control>

In the air conditioning operations (the cooling operation and the heating operation) described above, the air conditioning capacity of the outdoor unit 2 is controlled in such a way that the evaporation temperature  $T_e$  or the condensation temperature  $T_c$  of the refrigerant in the refrigerant circuit 10 becomes the target evaporation temperature  $T_{es}$  or the target condensation temperature  $T_{cs}$ . Furthermore, the devices and valves 41a, 41b, 44a, and 44b of the indoor units 4a and 4b are controlled in such a way that the room temperatures  $T_{ra}$  and  $T_{rb}$  associated with the indoor units 4a and 4b become the set temperatures  $T_{ras}$  and  $T_{rbs}$  of the room temperatures associated with the indoor units 4a and 4b. The setting of the set

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temperatures  $T_{ras}$  and  $T_{rbs}$  of the room temperatures associated with the indoor units **4a** and **4b** is performed by the remote controllers **49a** and **49b**. Furthermore, the control of the outdoor unit **2** is performed by the capacity controlling part **81**, which is configured by the outdoor-side control unit **38** of the control unit **8**, and the control of the indoor units **4a** and **4b** is performed by the indoor controlling part **82**, which is configured by the indoor-side control units **48a** and **48b** of the control unit **8**.

—During Cooling Operation—

In a case where the air conditioning operation is the cooling operation, the indoor controlling part **82** of the control unit **8** controls the opening degrees of the indoor expansion valves **41a** and **41b** in such a way that degrees of superheating  $SH_{ra}$  and  $SH_{rb}$  of the refrigerant in the outlets of the indoor heat exchangers **42a** and **42b** become target degrees of superheating  $SH_{ras}$  and  $SH_{rbs}$  (hereinafter this control will be called “degree of superheating control by indoor expansion valves”). Here, the degrees of superheating  $SH_{ra}$  and  $SH_{rb}$  are calculated from the suction pressure  $P_s$  detected by the suction pressure sensor **31** and the temperatures  $T_{rga}$  and  $T_{rgb}$  of the refrigerant on the gas sides of the indoor heat exchangers **42a** and **42b** detected by the gas-side temperature sensors **46a** and **46b**. More specifically, first, the suction pressure  $P_s$  is converted into the saturation temperature of the refrigerant to obtain the evaporation temperature  $T_e$ , which is a state quantity that is equivalent to the evaporation pressure  $P_e$  in the refrigerant circuit **10**. Here, “evaporation pressure  $P_e$ ” means a pressure representing the low-pressure refrigerant flowing from the outlets of the indoor expansion valves **41a** and **41b** via the indoor heat exchangers **42a** and **42b** to the suction side of the compressor **21** during the cooling operation. Additionally, the degrees of superheating  $SH_{ra}$  and  $SH_{rb}$  are obtained by subtracting the evaporation temperature  $T_e$  from the temperatures  $T_{rga}$  and  $T_{rgb}$  of the refrigerant on the gas sides of the indoor heat exchangers **42a** and **42b**.

Furthermore, in a case where the air conditioning operation is the cooling operation, the capacity controlling part **81** of the control unit **8** controls the operating capacity of the compressor **21** in such a way that the evaporation temperature  $T_e$  corresponding to the evaporation pressure  $P_e$  in the refrigerant circuit **10** becomes closer to the target evaporation temperature  $T_{es}$  (hereinafter this control will be called “evaporation temperature control by compressor”). Here, the control of the operating capacity of the compressor **21** is performed by changing the frequency of the compressor motor **20**. Furthermore, here, the evaporation temperature  $T_e$  is used as the state quantity that is controlled, but the state quantity that is controlled may also be the evaporation pressure  $P_e$ . In this case, it suffices to use a target evaporation pressure  $P_{es}$  corresponding to the target evaporation temperature  $T_{es}$ . That is, “evaporation pressure  $P_e$ ” and “evaporation temperature  $T_e$ ”, and “target evaporation pressure  $P_{es}$ ” and “target evaporation temperature  $T_{es}$ ”, mean substantially the same state quantities even though the wordings themselves are different.

In this way, in the cooling operation, the degree of superheating control by the indoor expansion valves **41a** and **41b** and the evaporation temperature control by the compressor **21** are performed as the basic control. Additionally, in the air conditioning apparatus **1**, it is ensured by this basic control of the cooling operation that the room temperatures  $T_{ra}$  and  $T_{rb}$  associated with the indoor units **4a** and **4b** become the set temperatures  $T_{ras}$  and  $T_{rbs}$  of the room temperatures associated with the indoor units **4a** and **4b**.

—During Heating Operation—

In a case where the air conditioning operation is the heating operation, the indoor controlling part **82** of the control unit **8**

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controls the opening degrees of the indoor expansion valves **41a** and **41b** in such a way that degrees of subcooling  $SC_{ra}$  and  $SC_{rb}$  of the refrigerant in the outlets of the indoor heat exchangers **42a** and **42b** become target degrees of subcooling  $SC_{ras}$  and  $SC_{rbs}$  (hereinafter this control will be called “degree of subcooling control by indoor expansion valves”). Here, the degrees of subcooling  $SC_{ra}$  and  $SC_{rb}$  are calculated from the discharge pressure  $P_d$  detected by the discharge pressure sensor **32** and the temperatures  $T_{rla}$  and  $T_{rlb}$  of the refrigerant on the liquid sides of the indoor heat exchangers **42a** and **42b** detected by the liquid-side temperature sensors **45a** and **45b**. More specifically, first, the discharge pressure  $P_d$  is converted into the saturation temperature of the refrigerant to obtain the condensation temperature  $T_c$ , which is a state quantity that is equivalent to the condensation pressure  $P_c$  in the refrigerant circuit **10**. Here, “condensation pressure  $P_c$ ” means a pressure representing the high-pressure refrigerant flowing from the discharge side of the compressor **21** via the indoor heat exchangers **42a** and **42b** to the indoor expansion valves **41a** and **41b** during the heating operation. Additionally, the degrees of subcooling  $SC_{ra}$  and  $SC_{rb}$  are obtained by subtracting the temperatures  $T_{rla}$  and  $T_{rlb}$  of the refrigerant on the liquid sides of the indoor heat exchangers **42a** and **42b** from the condensation temperature  $T_c$ .

Furthermore, in a case where the air conditioning operation is the heating operation, the capacity controlling part **81** of the control unit **8** controls the operating capacity of the compressor **21** in such a way that the condensation temperature  $T_c$  corresponding to the condensation pressure  $P_c$  in the refrigerant circuit **10** becomes closer to the target condensation temperature  $T_{cs}$  (hereinafter this control will be called “condensation temperature control by compressor”). Here, the control of the operating capacity of the compressor **21** is performed by changing the frequency of the compressor motor **20**. Furthermore, here, the condensation temperature  $T_c$  is used as the state quantity that is controlled, but the state quantity that is controlled may also be the condensation pressure  $P_c$ . In this case, it suffices to use a target condensation pressure  $P_{cs}$  corresponding to the target condensation temperature  $T_{cs}$ . That is, “condensation pressure  $P_c$ ” and “condensation temperature  $T_c$ ”, and “target condensation pressure  $P_{cs}$ ” and “target condensation temperature  $T_{cs}$ ”, mean substantially the same state quantities even though the wordings themselves are different.

In this way, in the heating operation, the degree of subcooling control by the indoor expansion valves **41a** and **41b** and the condensation temperature control by the compressor **21** are performed as the basic control. Additionally, in the air conditioning apparatus **1**, it is ensured by this basic control of the heating operation that the room temperatures  $T_{ra}$  and  $T_{rb}$  associated with the indoor units **4a** and **4b** become the set temperatures  $T_{ras}$  and  $T_{rbs}$  of the room temperatures associated with the indoor units **4a** and **4b**.

—Thermostat Control—

When the room temperatures  $T_{ra}$  and  $T_{rb}$  associated with the indoor units **4a** and **4b** reach the set temperatures  $T_{ras}$  and  $T_{rbs}$  of the room temperatures associated with the indoor units **4a** and **4b** because of the basic control of the air conditioning operations (the cooling operation and the heating operation) described above, the following thermostat control is performed.

The thermostat control means setting a thermostat temperature range with respect to the set temperatures  $T_{ras}$  and  $T_{rbs}$  of the indoor units **4a** and **4b** and performing indoor thermostat OFF, indoor thermostat ON, outdoor thermostat OFF, and outdoor thermostat ON. Here, “indoor thermostat OFF” means suspending, in a case where the room tempera-

ture associated with an indoor unit performing an air conditioning operation has become the set temperature, the air conditioning operation of the corresponding indoor unit. That is, the indoor expansion valve of the corresponding indoor unit is closed to ensure that the refrigerant does not flow to the indoor heat exchanger. "Indoor thermostat ON" means resuming, in a case where the room temperature associated with an indoor unit in an indoor thermostat OFF state has deviated from the thermostat temperature range, the air conditioning operation of the corresponding indoor unit. That is, the indoor expansion valve of the corresponding indoor unit is opened (i.e., the degree of superheating control or the degree of subcooling control by the indoor expansion valve is performed) to ensure that the refrigerant flows to the indoor heat exchanger. "Outdoor thermostat OFF" means stopping the compressor 21 in a case where all the indoor units performing an air conditioning operation have switched to an indoor thermostat OFF state. Because of this, the flow of the refrigerant in the refrigerant circuit 10 stops, and the air conditioning apparatus 1 switches to a state in which the air conditioning operations are all substantially stopped even though an air conditioning operation command is being given. "Outdoor thermostat ON" means restarting the compressor 21 in a case where, in the outdoor thermostat OFF state, at least one indoor unit has switched to an indoor thermostat ON state. Because of this, the refrigerant flows in the refrigerant circuit 10, and the air conditioning apparatus 1 switches to a state in which the air conditioning operations are resumed. Here, "indoor thermostat OFF" and "indoor thermostat ON" are performed by the indoor controlling part 82 of the control unit 8, and "outdoor thermostat OFF" and "outdoor thermostat ON" are performed by the capacity controlling part 81 of the control unit 8.

### (3) Target Refrigerant Temperature Mode Setting and Actions in Each Mode

When the air conditioning apparatus 1 performs the air conditioning operations (the cooling operation and the heating operation) accompanied by the thermostat control described above, the room temperatures  $T_{ra}$  and  $T_{rb}$  associated with the indoor units 4a and 4b are controlled in such a way as to become the set temperatures  $T_{ras}$  and  $T_{rbs}$  of the room temperatures associated with the indoor units 4a and 4b.

Here, it is conceivable to configure the air conditioning apparatus to change the target evaporation temperature  $T_{es}$  and the target condensation temperature  $T_{cs}$  in accordance with the air conditioning load characteristics of the building, like in patent document 1. That is, it is conceivable for the air conditioning apparatus to lower, during the cooling operation, the target evaporation temperature  $T_{es}$  the larger the temperature difference is between the set temperatures  $T_{ras}$  and  $T_{rbs}$  and the outdoor temperature  $T_a$  and to raise, during the heating operation, the target condensation temperature  $T_{cs}$  the larger the temperature difference is between the set temperatures  $T_{ras}$  and  $T_{rbs}$  and the outdoor temperature  $T_a$ . Additionally, when the air conditioning apparatus changes the target evaporation temperature  $T_{es}$  or the target condensation temperature  $T_{cs}$  in this way, in a case where the air conditioning capacity requirement from the indoor units 4a and 4b is small, the target evaporation temperature  $T_{es}$  becomes higher and the target condensation temperature  $T_{cs}$  becomes lower, so an excess of the air conditioning capacity of the outdoor unit 2 is suppressed. Because of this, the frequency with which the indoor units 4a and 4b and the compressor 21 alternate between being operated and being stopped—that is, indoor thermostat ON/indoor thermostat

OFF, outdoor thermostat ON/outdoor thermostat OFF—can be reduced so that energy conservation can be improved.

However, on the other hand, the amount of time it takes until the room temperatures  $T_{ra}$  and  $T_{rb}$  of the air conditioned spaces to reach the set temperatures  $T_{ras}$  and  $T_{rbs}$  tends to become longer in correspondence to the more the air conditioning capacity of the outdoor unit 2 tends to be easily suppressed, and there is the concern that comfort will be compromised.

In this way, simply changing the target evaporation temperature  $T_{es}$  or the target condensation temperature  $T_{cs}$  in accordance with the air conditioning load characteristics of the building will not necessarily satisfy all users, because although users who prefer to conserve energy will be satisfied, users who prefer comfort will not be easily satisfied.

Therefore, here, in order to make it possible for priority to be given to energy conservation or for priority to be given to comfort according to the preference of the user, as shown in FIG. 2, the control unit 8 is disposed with the target refrigerant temperature mode setting part 83 for setting modes relating to the target evaporation temperature  $T_{es}$  or the target condensation temperature  $T_{cs}$ , such as setting whether to change or fix the target evaporation temperature  $T_{es}$  and the target condensation temperature  $T_{cs}$ . Here, the target refrigerant temperature mode setting part 83 is a memory disposed in the outdoor-side control unit 38 of the control unit 8 and can set the target refrigerant temperature mode to various modes relating to the target evaporation temperature  $T_{es}$  or the target condensation temperature  $T_{cs}$  by communication from an external device for performing various control settings of the air conditioning apparatus 1. The target refrigerant temperature mode setting part 83 is not limited to the part described above, and it suffices for the target refrigerant temperature mode setting part 83 to be a part that can set the target refrigerant temperature mode to various modes relating to the target evaporation temperature  $T_{es}$  and the target condensation temperature  $T_{cs}$ , such as, for example, a DIP switch disposed in the outdoor-side control unit 38.

Next, the various modes relating to the target evaporation temperature  $T_{es}$  and the target condensation temperature  $T_{cs}$  that are settable by the target refrigerant temperature mode setting part 83 and the actions in each mode will be described using FIG. 3 to FIG. 9. Here, FIG. 3 is a drawing showing the various modes relating to the target evaporation temperature  $T_{es}$  and the target condensation temperature  $T_{cs}$  that are settable. FIG. 4 is a flowchart showing control for correcting the target evaporation temperature  $T_{es}$  in a fast changing mode (or first changing mode) and a slow changing mode (or second changing mode). The fast changing mode includes a powerful mode (or first sub-mode) and a quick mode (or second sub-mode). FIG. 5 is a flowchart showing control for correcting the target condensation temperature  $T_{cs}$  in the slow changing mode and the fast changing mode (the quick mode and the powerful mode). FIG. 6 is a drawing showing temporal changes, from the start of the cooling operation, in the target evaporation temperature  $T_{es}$ , room temperatures  $T_r$ , and efficiency in a target refrigerant temperature fixing mode and a target refrigerant temperature changing mode (the slow changing mode, the quick mode, and the powerful mode). FIG. 7 is a drawing showing temporal changes in the target evaporation temperature  $T_{es}$  and the room temperatures  $T_r$  in the slow changing mode, the quick mode, and the powerful mode in a case where the number of indoor units in operation has increased during the cooling operation. FIG. 8 is a drawing showing temporal changes, from the start of the heating operation, in the target condensation temperature  $T_{cs}$ , the room temperatures  $T_r$ , and efficiency in the target refrigerant

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temperature fixing mode and the target refrigerant temperature changing mode (the slow changing mode, the quick mode, and the powerful mode). FIG. 9 is a drawing showing temporal changes in the target condensation temperature  $T_{cs}$  and the room temperatures  $T_r$  in the slow changing mode, the quick mode, and the powerful mode in a case where the number of indoor units in operation has increased during the heating operation.

#### <Target Refrigerant Temperature Fixing Mode>

First, as a mode relating to the target evaporation temperature  $T_{es}$  and the target condensation temperature  $T_{cs}$  that is settable by the target refrigerant temperature mode setting part 83, as shown in FIG. 3, there is a target refrigerant temperature fixing mode that fixes the target evaporation temperature  $T_{es}$  or the target condensation temperature  $T_{cs}$ . When the mode is set to the target refrigerant temperature fixing mode, the target evaporation temperature  $T_{es}$  in the cooling operation is fixed to a predetermined value and the target condensation temperature  $T_{cs}$  in the heating operation is fixed to a predetermined value.

Here, as shown in FIG. 2, the control unit 8 is disposed with the target refrigerant temperature changing part 84 serving as a part for changing or fixing the target evaporation temperature  $T_{es}$  and the target condensation temperature  $T_{cs}$  in accordance with the mode that has been set by the target refrigerant temperature mode setting part 83. For this reason, when the mode is set to the target refrigerant temperature fixing mode by the target refrigerant temperature mode setting part 83, the target refrigerant temperature changing part 84 fixes the target evaporation temperature  $T_{es}$  in the cooling operation to the predetermined value and fixes the target condensation temperature  $T_{cs}$  in the heating operation to the predetermined value.

Here, the target evaporation temperature  $T_{es}$  is fixed to a maximum capacity evaporation temperature  $T_{em}$  (e.g., 6°C.) corresponding to a case where the air conditioning (cooling) capacity of the outdoor unit 2 is at 100% capacity. Furthermore, the target condensation temperature  $T_{cs}$  is fixed to a maximum capacity condensation temperature  $T_{cm}$  (e.g., 46°C.) corresponding to a case where the air conditioning (heating) capacity of the outdoor unit 2 is at 100% capacity.

In the target refrigerant temperature fixing mode, the target evaporation temperature  $T_{es}$  or the target condensation temperature  $T_{cs}$  is constantly fixed to the maximum capacity evaporation temperature  $T_{em}$  or the maximum capacity condensation temperature  $T_{cm}$ .

Because of this, in a case where the mode is set to the target refrigerant temperature fixing mode, as shown in FIG. 6 and FIG. 8, the air conditioning operations can be performed in a state in which priority is constantly given to comfort. However, it becomes easy for efficiency to drop because it is easy for the air conditioning capacity of the outdoor unit 2 to become excessive.

#### <Target Refrigerant Temperature Changing Mode>

Next, as a mode relating to the target evaporation temperature  $T_{es}$  and the target condensation temperature  $T_{cs}$  that is settable by the target refrigerant temperature mode setting part 83, as shown in FIG. 3, there is a target refrigerant temperature changing mode that changes the target evaporation temperature  $T_{es}$  or the target condensation temperature  $T_{cs}$ . When the mode is set to the target refrigerant temperature changing mode, the target evaporation temperature  $T_{es}$  is changed as a result of a reference target evaporation temperature  $KTe_b$  serving as a reference value of the target evaporation temperature  $T_{es}$  in the cooling operation being set automatically or by the user and an evaporation temperature correction value  $KTec$  being added to the reference target

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evaporation temperature  $KTe_b$ . That is, the target evaporation temperature  $T_{es}$  can be expressed by the equation  $T_{es} = KTe_b + KTec$ . Furthermore, in the heating operation, the target condensation temperature  $T_{cs}$  is changed as a result of a reference target condensation temperature  $KTc_b$  serving as a reference value of the target condensation temperature  $T_{cs}$  being set automatically or by the user and a condensation temperature correction value  $KTcc$  being added to the reference target condensation temperature  $KTc_b$ . That is, the target condensation temperature  $T_{cs}$  can be expressed by the equation  $T_{cs} = KTc_b + KTcc$ .

Here, as shown in FIG. 3, the target refrigerant temperature changing mode has two modes (a fast changing mode and a slow changing mode) in which the degree of control trackability is different. Additionally, the fast changing mode and the slow changing mode are set by the target refrigerant temperature mode setting part 83. Furthermore, as shown in FIG. 3, the fast changing mode has two modes (a powerful mode and a quick mode) in which the degree of control trackability is further different. Additionally, the powerful mode and the quick mode are set by the target refrigerant temperature mode setting part 83. Furthermore, the target refrigerant temperature changing mode has two modes, i.e., an automatic mode and a high-sensitivity mode (or user-set mode), in which the way of setting the reference target evaporation temperature  $KTe_b$  or the reference target condensation temperature  $KTc_b$  is different. Additionally, the automatic mode or the high-sensitivity mode is set, together with the fast changing mode and the slow changing mode, by the target refrigerant temperature mode setting part 83. Moreover, as shown in FIG. 3, the target refrigerant temperature changing mode has an economy mode in which the reference target evaporation temperature  $KTe_b$  or the reference target condensation temperature  $KTc_b$  that has been set in the high-sensitivity mode is set as the target evaporation temperature  $T_{es}$  or the target condensation temperature  $T_{cs}$  without a correction being made to that reference target evaporation temperature  $KTe_b$  or that reference target condensation temperature  $KTc_b$ . Additionally, the economy mode is set, together with the automatic mode or the high-sensitivity mode, by the target refrigerant temperature mode setting part 83.

In this way, here, the mode can be set to either of the target refrigerant temperature changing mode and the target refrigerant temperature fixing mode by the target refrigerant temperature mode setting part 83. Additionally, when the mode is set to the target refrigerant temperature changing mode, priority can be given to energy conservation as described below, and when the mode is set to the target refrigerant temperature fixing mode, priority can be given to comfort as described above. Because of this, here, priority can be given to energy conservation or priority can be given to comfort according to the preference of the user.

#### —Automatic Mode—

In the automatic mode, the reference target evaporation temperature  $KTe_b$  or the reference target condensation temperature  $KTc_b$  is set in accordance with the outdoor temperature  $T_a$  of the outside space where the outdoor unit 2 is disposed. Specifically, when the mode is set to the automatic mode by the target refrigerant temperature mode setting part 83, the reference target evaporation temperature  $KTe_b$  or the reference target condensation temperature  $KTc_b$  is set on the basis of a function of the outdoor temperature  $T_a$ . In the cooling operation, more air conditioning (cooling) capacity tends to be required the higher the outdoor temperature  $T_a$  is, so the reference target evaporation temperature  $KTe_b$  is set on the basis of a function in which the reference target evaporation temperature  $KTe_b$  becomes lower as the outdoor tem-

perature  $T_a$  becomes higher. Furthermore, in the heating operation, more air conditioning (heating) capacity tends to be required the lower the outdoor temperature  $T_a$  is, so the reference target condensation temperature  $KT_{cb}$  is set on the basis of a function in which the reference target condensation temperature  $KT_{cb}$  becomes higher as the outdoor temperature  $T_a$  becomes lower. For this reason, when the mode is set to the automatic mode by the target refrigerant temperature mode setting part **83**, the target refrigerant temperature changing part **84** automatically sets the reference target evaporation temperature  $KT_{eb}$  in the cooling operation to a temperature value obtained on the basis of the above-described function and the outdoor temperature  $T_a$  and automatically sets the reference target condensation temperature  $KT_{cb}$  in the heating operation to a temperature value obtained on the basis of the above-described function and the outdoor temperature  $T_a$ .

Additionally, in the automatic mode, during the cooling operation and the heating operation, the target refrigerant temperature changing part **84** changes the target evaporation temperature  $T_{es}$  and the target condensation temperature  $T_{cs}$  by changing the reference target evaporation temperature  $KT_{eb}$  and the reference target condensation temperature  $KT_{cb}$  in accordance with the outdoor temperature  $T_a$  and at the same time further making a correction according to the slow changing mode and the fast changing mode described below.

(Slow Changing Mode)

When the mode is set to the automatic mode and is set to the slow changing mode by the target refrigerant temperature mode setting part **83**, during the cooling operation, the evaporation temperature correction value  $KT_{ec}$  is changed as shown in steps ST1 to ST4 of FIG. 4. Additionally, the target evaporation temperature  $T_{es}$  is changed by making a correction that adds the evaporation temperature correction value  $KT_{ec}$  to the reference target evaporation temperature  $KT_{eb}$ . The changing of the evaporation temperature correction value  $KT_{ec}$  in the slow changing mode and the control that corrects the target evaporation temperature  $T_{es}$  by adding the evaporation temperature correction value  $KT_{ec}$  to the reference target evaporation temperature  $KT_{eb}$  are performed by the target refrigerant temperature changing part **84**.

Specifically, at the time when the cooling operation is started, first, in step ST1, an initial value setting of the evaporation temperature correction value  $KT_{ec}$  is performed. Here, the evaporation temperature correction value  $KT_{ec}=0$ , and so because of this, the target evaporation temperature  $T_{es}$ =the reference target evaporation temperature  $KT_{eb}$ . Because of this, the cooling operation is started using the reference target evaporation temperature  $KT_{eb}$  as the target evaporation temperature  $T_{es}$ .

Then, after performing processing that maintains the current state in step ST2, the target refrigerant temperature changing part **84** moves to the processing of step ST3 or step ST4.

In step ST3, assuming that a first amount of waiting time  $t1$  (e.g., 10 minutes) has passed since the move to step ST2 and that a moving condition of step ST5 described later has not been met, the target refrigerant temperature changing part **84** performs slow changing control that changes the target evaporation temperature  $T_{es}$  in accordance with the temperature differences ( $Tr-Trs$ ) between the room temperatures  $Tr$  and  $Trb$  (hereinafter called "the room temperatures  $Tr$ " by omitting the letters "a" and "b") of the air conditioned spaces targeted by the indoor units **4a** and **4b** and the set temperatures  $Tras$  and  $Trbs$  (hereinafter called "the set temperatures  $Trs$ " by omitting the letters "a" and "b") that are target values

of the room temperatures  $Tr$ . Here, in a case where the target refrigerant temperature changing part **84** has determined that the temperature differences ( $Tr-Trs$ ) meet the condition that it is necessary to lower the target evaporation temperature  $T_{es}$ , the target refrigerant temperature changing part **84** reduces the evaporation temperature correction value  $KT_{ec}$  by subtracting a correction value  $\Delta Tec1$  (e.g.,  $0.5^\circ\text{C}$ .) from the current evaporation temperature correction value  $KT_{ec}$  and adds the evaporation temperature correction value  $KT_{ec}$  to the reference target evaporation temperature  $KT_{eb}$  to thereby correct the target evaporation temperature  $T_{es}$  in such a way that the target evaporation temperature  $T_{es}$  becomes lower.

Here, as a condition of the temperature differences ( $Tr-Trs$ ), in a case where, compared to ( $Tr-Trs$ ) $_{max}$  that is a maximum of the temperature differences ( $Tr-Trs$ ) among the indoor units in an indoor thermostat ON state, ( $Tr-Trs$ ) $_{max}$  an amount of time  $t2$  (e.g., 5 minutes) before is equal to or less than a predetermined temperature difference  $\Delta Tre1$  (e.g.,  $0.2^\circ\text{C}$ .), the target refrigerant temperature changing part **84** performs slow changing control that corrects the target evaporation temperature  $T_{es}$  in such a way that the target evaporation temperature  $T_{es}$  becomes lower. That is, in a case where a large change cannot be seen in the room temperatures  $Tr$ , the target refrigerant temperature changing part **84** determines that the temperature differences ( $Tr-Trs$ ) meet the condition that it is necessary to lower the target evaporation temperature  $T_{es}$ . Furthermore, as a condition of the temperature differences ( $Tr-Trs$ ), also in a case where ( $Tr-Trs$ ) $_{max}$  that is a maximum of the temperature differences ( $Tr-Trs$ ) among the indoor units in an indoor thermostat ON state is larger than a predetermined temperature difference  $\Delta Tre2$  (e.g.,  $3^\circ\text{C}$ .), the target refrigerant temperature changing part **84** performs slow changing control that corrects the target evaporation temperature  $T_{es}$  in such a way that the target evaporation temperature  $T_{es}$  becomes lower. That is, in a case where the room temperatures  $Tr$  are higher than the set temperatures  $Trs$ , the target refrigerant temperature changing part **84** determines that the temperature differences ( $Tr-Trs$ ) meet the condition that it is necessary to lower the target evaporation temperature  $T_{es}$ .

In step ST4, assuming that the first amount of waiting time  $t1$  (e.g., 10 minutes) has passed since the move to step ST2, the target refrigerant temperature changing part **84** performs slow changing control that changes the target evaporation temperature  $T_{es}$  in accordance with the temperature differences ( $Tr-Trs$ ) between the room temperatures  $Tr$  of the air conditioned spaces targeted by the indoor units **4a** and **4b** and the set temperatures  $Trs$  that are target values of the room temperatures  $Tr$ . Here, in a case where the target refrigerant temperature changing part **84** has determined that the temperature differences ( $Tr-Trs$ ) meet the condition that it is necessary to raise the target evaporation temperature  $T_{es}$ , the target refrigerant temperature changing part **84** increases the evaporation temperature correction value  $KT_{ec}$  by adding a correction value  $\Delta Tec2$  (e.g.,  $1^\circ\text{C}$ .) to the current evaporation temperature correction value  $KT_{ec}$  and adds the evaporation temperature correction value  $KT_{ec}$  to the reference target evaporation temperature  $KT_{eb}$  to thereby correct the target evaporation temperature  $T_{es}$  in such a way that the target evaporation temperature  $T_{es}$  becomes higher.

Here, as a condition of the temperature differences ( $Tr-Trs$ ), in a case where, compared to ( $Tr-Trs$ ) $_{max}$  that is a maximum of the temperature differences ( $Tr-Trs$ ) among the indoor units in an indoor thermostat ON state, ( $Tr-Trs$ ) $_{max}$  the amount of time  $t2$  (e.g., 5 minutes) before is larger than a predetermined temperature difference  $\Delta Tre3$  (e.g.,  $0.5^\circ\text{C}$ .),

the target refrigerant temperature changing part **84** performs slow changing control that corrects the target evaporation temperature  $T_{es}$  in such a way that the target evaporation temperature  $T_{es}$  becomes higher. That is, in a case where the room temperatures  $T_r$  are tending to become lower, the target refrigerant temperature changing part **84** determines that the temperature differences  $(T_r - T_{rs})$  meet the condition that it is necessary to raise the target evaporation temperature  $T_{es}$ . Furthermore, as a condition of the temperature differences  $(T_r - T_{rs})$ , also in a case where  $(T_r - T_{rs})_{\max}$  that is a maximum of the temperature differences  $(T_r - T_{rs})$  among the indoor units in an indoor thermostat ON state is equal to or less than a predetermined temperature difference  $\Delta T_{re4}$  (e.g.,  $0.5^\circ \text{C}$ .), the target refrigerant temperature changing part **84** performs slow changing control that corrects the target evaporation temperature  $T_{es}$  in such a way that the target evaporation temperature  $T_{es}$  becomes higher. That is, in a case where the room temperatures  $T_r$  are in the vicinity of or lower than the set temperatures  $T_{rs}$ , the target refrigerant temperature changing part **84** determines that the temperature differences  $(T_r - T_{rs})$  meet the condition that it is necessary to raise the target evaporation temperature  $T_{es}$ .

Then, after performing the processing of step ST3 or step ST4, the target refrigerant temperature changing part **84** returns to the processing of step ST2, and thereafter the processing of steps ST2, ST3, and ST4 is repeated.

Because of this slow changing mode, that is to say the slow changing control resulting from steps ST2, ST3, and ST4 during the cooling operation, the target evaporation temperature  $T_{es}$  is slowly changed as shown in FIG. 6. For this reason, an excess of the air conditioning (cooling) capacity of the outdoor unit **2** can be suppressed, efficiency is more easily improved, and energy conservation can be improved.

Moreover, here, the reference target evaporation temperature  $K_{Teb}$  is set in accordance with the outdoor temperature  $T_a$  by the automatic mode, so the target evaporation temperature  $T_{es}$  that is set as a result of a correction corresponding to the slow changing mode being made to the reference target evaporation temperature  $K_{Teb}$  can further improve the degree of energy conservation.

Moreover, here, the maximum value of the temperature differences between the room temperatures  $T_r$  and the set temperatures  $T_{rs}$  among the indoor units in operation (in an indoor thermostat ON state) is used as a condition for changing the target evaporation temperature  $T_{es}$ . For this reason, the target evaporation temperature  $T_{es}$  is changed in accordance with the indoor unit in which the largest air conditioning (cooling) capacity is required. Because of this, here, the target evaporation temperature  $T_{es}$  can be promptly changed and control trackability can be improved.

Furthermore, when the mode is set to the automatic mode and is set to the slow changing mode by the target refrigerant temperature mode setting part **83**, during the heating operation, the condensation temperature correction value  $K_{Tcc}$  is changed as shown in steps ST11 to ST14 of FIG. 5. Additionally, the target condensation temperature  $T_{cs}$  is changed by making a correction that adds the condensation temperature correction value  $K_{Tcc}$  to the reference target condensation temperature  $K_{Tcb}$ . The changing of the condensation temperature correction value  $K_{Tcc}$  and the control that corrects the target condensation temperature  $T_{cs}$  by adding the condensation temperature correction value  $K_{Tcc}$  to the reference target condensation temperature  $K_{Tcb}$  are performed by the target refrigerant temperature changing part **84**.

Specifically, at the time when the heating operation is started, first, in step ST11, an initial value setting of the condensation temperature correction value  $K_{Tcc}$  is per-

formed. Here, the condensation temperature correction value  $K_{Tcc}=0$ , and so because of this, the target condensation temperature  $T_{cs}=\text{the reference target condensation temperature } K_{Tcb}$ . Because of this, the heating operation is started using the reference target condensation temperature  $K_{Tcb}$  as the target condensation temperature  $T_{cs}$ .

Then, after performing processing that maintains the current state in step ST12, the target refrigerant temperature changing part **84** moves to the processing of step ST13 or step ST14.

In step ST13, assuming that a first amount of waiting time  $t_1$  (e.g., 10 minutes) has passed since the move to step ST12 and that a moving condition of step ST15 described later has not been met, the target refrigerant temperature changing part **84** performs slow changing control that changes the target condensation temperature  $T_{cs}$  in accordance with the temperature differences  $(T_{rs} - T_r)$  between the room temperatures  $T_r$  of the air conditioned spaces targeted by the indoor units **4a** and **4b** and the set temperatures  $T_{rs}$  that are target values of the room temperatures  $T_r$ . Here, in a case where the target refrigerant temperature changing part **84** has determined that the temperature differences  $(T_{rs} - T_r)$  meet the condition that it is necessary to raise the target condensation temperature  $T_{cs}$ , the target refrigerant temperature changing part **84** increases the condensation temperature correction value  $K_{Tcc}$  by adding a correction value  $\Delta T_{cc1}$  (e.g.,  $1^\circ \text{C}$ .) to the current condensation temperature correction value  $K_{Tcc}$  and adds the condensation temperature correction value  $K_{Tcc}$  to the reference target condensation temperature  $K_{Tcb}$  to thereby correct the target condensation temperature  $T_{cs}$  in such a way that the target condensation temperature  $T_{cs}$  becomes higher.

Here, as a condition of the temperature differences  $(T_{rs} - T_r)$ , in a case where, compared to  $(T_{rs} - T_r)_{\max}$  that is a maximum of the temperature differences  $(T_{rs} - T_r)$  among the indoor units in an indoor thermostat ON state,  $(T_{rs} - T_r)_{\max}$  an amount of time  $t_2$  (e.g., 5 minutes) before is equal to or less than a predetermined temperature difference  $\Delta T_{rc1}$  (e.g.,  $0.2^\circ \text{C}$ .), the target refrigerant temperature changing part **84** performs slow changing control that corrects the target condensation temperature  $T_{cs}$  in such a way that the target condensation temperature  $T_{cs}$  becomes higher. That is, in a case where a large change cannot be seen in the room temperatures  $T_r$ , the target refrigerant temperature changing part **84** determines that the temperature differences  $(T_{rs} - T_r)$  meet the condition that it is necessary to raise the target condensation temperature  $T_{cs}$ . Furthermore, as a condition of the temperature differences  $(T_{rs} - T_r)$ , also in a case where  $(T_{rs} - T_r)_{\max}$  that is a maximum of the temperature differences  $(T_{rs} - T_r)$  among the indoor units in an indoor thermostat ON state is larger than a predetermined temperature difference  $\Delta T_{rc2}$  (e.g.,  $3^\circ \text{C}$ .), the target refrigerant temperature changing part **84** performs slow changing control that corrects the target condensation temperature  $T_{cs}$  in such a way that the target condensation temperature  $T_{cs}$  becomes higher. That is, in a case where the room temperatures  $T_r$  are lower than the set temperatures  $T_{rs}$ , the target refrigerant temperature changing part **84** determines that the temperature differences  $(T_{rs} - T_r)$  meet the condition that it is necessary to raise the target condensation temperature  $T_{cs}$ .

In step ST14, assuming that the first amount of waiting time  $t_1$  (e.g., 10 minutes) has passed since the move to step ST12, the target refrigerant temperature changing part **84** performs slow changing control that changes the target condensation temperature  $T_{cs}$  in accordance with the temperature differences  $(T_{rs} - T_r)$  between the room temperatures  $T_r$  of the air conditioned spaces targeted by the indoor units **4a**



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and 4b and the set temperatures  $Trs$  that are target values of the room temperatures  $Tr$ . Here, in a case where the target refrigerant temperature changing part 84 has determined that the temperature differences  $(Trs-Tr)$  meet the condition that it is necessary to lower the target condensation temperature  $Tcs$ , the target refrigerant temperature changing part 84 reduces the condensation temperature correction value  $KTec$  by subtracting a correction value  $\Delta Tcc2$  (e.g.,  $1.5^\circ C.$ ) from the current condensation temperature correction value  $KTec$  and adds the condensation temperature correction value  $KTec$  to the reference target condensation temperature  $KTcb$  to thereby correct the target condensation temperature  $Tcs$  in such a way that the target condensation temperature  $Tcs$  becomes lower.

Here, as a condition of the temperature differences  $(Trs-Tr)$ , also in a case where  $(Trs-Tr)_{max}$  that is a maximum of the temperature differences  $(Trs-Tr)$  among the indoor units in an indoor thermostat ON state is equal to or less than a predetermined temperature difference  $\Delta Trc3$  (e.g.,  $1.5^\circ C.$ ), the target refrigerant temperature changing part 84 performs slow changing control that corrects the target condensation temperature  $Tcs$  in such a way that the target condensation temperature  $Tcs$  becomes lower. That is, in a case where the room temperatures  $Tr$  are in the vicinity of or higher than the set temperatures  $Trs$ , the target refrigerant temperature changing part 84 determines that the temperature differences  $(Trs-Tr)$  meet the condition that it is necessary to lower the target condensation temperature  $Tcs$ .

Then, after performing the processing of step ST13 or step ST14, the target refrigerant temperature changing part 84 returns to the processing of step ST12, and thereafter the processing of steps ST12, ST13, and ST14 is repeated.

Because of this slow changing mode, that is to say the slow changing control resulting from steps ST12, ST13, and ST14 during the heating operation, the target condensation temperature  $Tcs$  is slowly changed as shown in FIG. 8. For this reason, basically an excess of the air conditioning (heating) capacity of the outdoor unit 2 can be suppressed, efficiency is more easily improved, and energy conservation can be improved.

Moreover, here, the reference target condensation temperature  $KTcb$  is set in accordance with the outdoor temperature  $Ta$  by the automatic mode, so the target condensation temperature  $Tcs$  that is set as a result of a correction corresponding to the slow changing mode being made to the reference target condensation temperature  $KTcb$  can further improve the degree of energy conservation.

Moreover, here, the maximum value of the temperature differences between the room temperatures  $Tr$  and the set temperatures  $Trs$  among the indoor units in operation (in an indoor thermostat ON state) is used as a condition for changing the target condensation temperature  $Tcs$ . For this reason, the target condensation temperature  $Tcs$  is changed in accordance with the indoor unit in which the largest air conditioning (heating) capacity is required. Because of this, here, the target condensation temperature  $Tcs$  can be promptly changed and control trackability can be improved. (Fast Changing Mode)

When the mode is set to the automatic mode and is set to the fast changing mode by the target refrigerant temperature mode setting part 83, during the cooling operation, the same slow changing control resulting from steps ST1 to ST4 as in the slow changing mode described above is performed, and in a case where the temperature differences  $(Tr-Trs)$  have exceeded a threshold temperature difference and the number of indoor units in operation has increased, as shown in step ST5 of FIG. 4, fast changing control is performed where the

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evaporation temperature correction value  $KTec$  and the target evaporation temperature  $Tes$  are forcibly changed to fast tracking evaporation temperatures (here, the maximum capacity evaporation temperature  $Tem$  and a lowest evaporation temperature  $Teex$ ).

Specifically, in step ST5, assuming that the first amount of waiting time  $t1$  (e.g., 10 minutes) has passed since the move to step ST2, in a case where  $(Tr-Trs)_{max}$  that is a maximum of the temperature differences  $(Tr-Trs)$  among the indoor units in an indoor thermostat ON state is larger than the predetermined temperature difference  $\Delta Tre2$  (e.g.,  $3^\circ C.$ ) serving as a threshold temperature difference and the current number of indoor units in an indoor thermostat ON state is larger than the number of indoor units in an indoor thermostat ON state an amount of time  $t3$  (e.g., 30 seconds) before, the target refrigerant temperature changing part 84 performs fast changing control that corrects the target evaporation temperature  $Tes$  in such a way as to rapidly lower the target evaporation temperature  $Tes$ . That is, in a case where the number of indoor units in operation has increased (also including a case where an indoor unit in an indoor thermostat OFF state has switched to a thermostat ON state), a large air conditioning (cooling) capacity becomes necessary in the outdoor unit 2, and the target refrigerant temperature changing part 84 determines that this meets the condition that it is necessary to rapidly lower the target evaporation temperature  $Tes$ .

Here, the fast changing mode has a powerful mode and a quick mode. Additionally, in the powerful mode, in the case meeting the condition that it is necessary to rapidly lower the target evaporation temperature  $Tes$ , powerful changing control is performed which changes the evaporation temperature correction value  $KTec$  by subtracting the reference target evaporation temperature  $KTeb$  from the current evaporation temperature correction value  $KTec$  and adding a fast tracking evaporation temperature (here, a lowest evaporation temperature  $Teex$  exceeding the maximum capacity evaporation temperature  $Tem$ ) and adds the evaporation temperature correction value  $Tec$  to the reference target evaporation temperature  $KTeb$  to thereby forcibly change the target evaporation temperature  $Tes$  to the lowest evaporation temperature  $Teex$  (e.g.,  $3^\circ C.$ ) serving as the fast tracking evaporation temperature. That is, the powerful mode is a mode that allows the target evaporation temperature  $Tes$  to be changed to the lowest evaporation temperature  $Teex$  exceeding the maximum capacity evaporation temperature  $Tem$ . Furthermore, in the quick mode, in the case meeting the condition that it is necessary to rapidly lower the target evaporation temperature  $Tes$ , quick changing control is performed which changes the evaporation temperature correction value  $KTec$  by subtracting the reference target evaporation temperature  $KTeb$  from the current evaporation temperature correction value  $KTec$  and adding a fast tracking evaporation temperature (here, a maximum capacity evaporation temperature  $Tem$ ) and adds the evaporation temperature correction value  $KTec$  to the reference target evaporation temperature  $KTeb$  to thereby forcibly change the target evaporation temperature  $Tes$  to the maximum capacity evaporation temperature  $Tem$  (e.g.,  $6^\circ C.$ ) serving as the fast tracking evaporation temperature. That is, the quick mode is a mode that does not allow the target evaporation temperature  $Tes$  to be changed to the lowest evaporation temperature  $Teex$ . The changing of the evaporation temperature correction value  $KTec$  in the fast changing mode (the powerful mode and the quick mode) and the control that corrects the target evaporation temperature  $Tes$  by adding the evaporation temperature correction value  $KTec$  to



the reference target evaporation temperature  $K_{Teb}$  are also performed by the target refrigerant temperature changing part **84**.

Then, after performing the processing of step **ST5**, the target refrigerant temperature changing part **84** returns to the processing of step **ST2**, and thereafter the processing of steps **ST2**, **ST3**, **ST4**, and **ST5** is repeated.

Because of this fast changing mode, that is to say the fast changing control resulting from steps **ST2**, **ST3**, **ST4**, and **ST5** during the cooling operation, as shown in FIG. 6, the target evaporation temperature  $T_{es}$  is changed in such a way that the room temperatures  $T_r$  reach the set temperatures  $T_{rs}$  in a shorter amount of time compared to the case resulting from the slow changing mode (i.e., in the slow changing mode, the target evaporation temperature  $T_{es}$  is changed in such a way that the room temperatures  $T_r$  reach the set temperatures  $T_{rs}$  in a longer amount of time than in the fast changing mode). For this reason, by setting the mode to the fast changing mode, control trackability can be improved compared to a case where the mode is set to the slow changing mode. Because of this, here, by setting the mode to the target refrigerant temperature changing mode, priority can be given to energy conservation, and at the same time the degree of control trackability can be changed according to the preference of the user.

Furthermore, here, in cases other than a case where the temperature differences between the room temperatures  $T_r$  and the set temperatures  $T_{rs}$  exceed the threshold temperature difference (here, the predetermined temperature difference  $\Delta T_{re2}$ ) and the number of indoor units in operation increases, the target evaporation temperature  $T_{es}$  is slowly changed by step **ST3**. For this reason, basically an excess of the air conditioning (cooling) capacity of the outdoor unit **2** can be suppressed. Moreover, here, in a case where the temperature differences between the room temperatures  $T_r$  and the set temperatures  $T_{rs}$  exceed the threshold temperature difference (here, the predetermined temperature difference  $\Delta T_{re2}$ ) and the number of indoor units in operation increases, that is to say a case where a large air conditioning (cooling) capacity becomes necessary in the outdoor unit **2** as a result of the number of indoor units in operation increasing, as shown in FIG. 7, the target evaporation temperature  $T_{es}$  is changed to a fast tracking evaporation temperature (here, the maximum capacity evaporation temperature  $T_{em}$  and the lowest evaporation temperature  $T_{ex}$ ) by performing fast changing control. Because of this, here, by changing the target evaporation temperature  $T_{es}$ , energy conservation can be improved, and sufficient control trackability can be obtained even in a case where the number of indoor units in operation increases.

Furthermore, here, the reference target evaporation temperature  $K_{Teb}$  is set in accordance with the outdoor temperature  $T_a$  by the automatic mode, so the target evaporation temperature  $T_{es}$  that is set as a result of a correction corresponding to the fast changing mode being made to the reference target evaporation temperature  $K_{Teb}$  can further improve the degree of energy conservation.

Furthermore, here, the maximum value of the temperature differences between the room temperatures  $T_r$  and the set temperatures  $T_{rs}$  among the indoor units in operation (in an indoor thermostat ON state) is used as a condition for changing the target evaporation temperature  $T_{es}$ . For this reason, the target evaporation temperature  $T_{es}$  is changed in accordance with the indoor unit in which the largest air conditioning (cooling) capacity is required. Because of this, here, the target evaporation temperature  $T_{es}$  can be promptly changed and control trackability can be improved.

Furthermore, here, the fast changing mode (fast changing control) can be set to either of two modes (control)—the powerful mode (powerful changing control) and the quick mode (quick changing control)—in which the degree of control trackability is further different. Additionally, when the mode is set to the powerful mode, the target evaporation temperature  $T_{es}$  is allowed to be changed to the lowest evaporation temperature  $T_{ex}$  exceeding the maximum capacity evaporation temperature  $T_{em}$ , so as shown in FIG. 7, control trackability is further improved compared to a case where the mode is set to the quick mode or a case where the mode is set to the target refrigerant temperature fixing mode. Because of this, here, by setting the mode to the fast changing mode, control trackability can be improved, and at the same time the degree of control trackability can be further changed according to the preference of the user.

Furthermore, when the mode is set to the automatic mode and is set to the fast changing mode by the target refrigerant temperature mode setting part **83**, during the heating operation, the same slow changing control resulting from steps **ST11** to **ST14** as in the slow changing mode described above is performed, and in a case where the temperature differences ( $T_{rs} - T_r$ ) have exceeded the threshold temperature difference and the number of indoor units in operation has increased, as shown in step **ST15** of FIG. 5, fast changing control is performed in which the condensation temperature correction value  $K_{Tcc}$  and the target condensation temperature  $T_{cs}$  are forcibly changed to fast tracking condensation temperatures (here, the maximum capacity condensation temperature  $T_{cm}$  and a highest condensation temperature  $T_{cex}$ ).

Specifically, in step **ST15**, assuming that the first amount of waiting time  $t_1$  (e.g., 10 minutes) has passed since the move to step **ST12**, in a case where  $(T_{rs} - T_r)_{\max}$  that is a maximum of the temperature differences ( $T_{rs} - T_r$ ) among the indoor units in an indoor thermostat ON state is larger than the predetermined temperature difference  $\Delta T_{rc2}$  (e.g., 3° C.) serving as a threshold temperature difference and the current number of indoor units in an indoor thermostat ON state is larger than the number of indoor units in an indoor thermostat ON state an amount of time  $t_3$  (e.g., 30 seconds) before, the target refrigerant temperature changing part **84** performs fast changing control that corrects the target condensation temperature  $T_{cs}$  in such a way as to rapidly raise the target condensation temperature  $T_{cs}$ . That is, in a case where the number of indoor units in operation has increased (also including a case where an indoor unit in an indoor thermostat OFF state has switched to a thermostat ON state), a large air conditioning (heating) capacity becomes necessary in the outdoor unit **2**, and the target refrigerant temperature changing part **84** determines that this meets the condition that it is necessary to rapidly raise the target condensation temperature  $T_{cs}$ .

Here, the fast changing mode has a powerful mode and a quick mode. Additionally, in the powerful mode, in the case meeting the condition that it is necessary to rapidly raise the target condensation temperature  $T_{cs}$ , powerful changing control is performed which changes the condensation temperature correction value  $K_{Tcc}$  by subtracting the reference target condensation temperature  $K_{Tcb}$  from the current condensation temperature correction value  $K_{Tcc}$  and adding a fast tracking condensation temperature (here, a highest condensation temperature  $T_{cex}$  exceeding the maximum capacity condensation temperature  $T_{cm}$ ) and adds the condensation temperature correction value  $K_{Tcc}$  to the reference target condensation temperature  $K_{Tcb}$  to thereby forcibly change the target condensation temperature  $T_{cs}$  to the highest condensation temperature  $T_{cex}$  (e.g., 49° C.) serving as the fast

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tracking condensation temperature. That is, the powerful mode is a mode that allows the target condensation temperature  $T_{cs}$  to be changed to the highest condensation temperature  $T_{cex}$  exceeding the maximum capacity condensation temperature  $T_{cm}$ . Furthermore, in the quick mode, in the case meeting the condition that it is necessary to rapidly raise the target condensation temperature  $T_{cs}$ , quick changing control is performed which changes the condensation temperature correction value  $KT_{cc}$  by subtracting the reference target condensation temperature  $KT_{cb}$  from the current condensation temperature correction value  $KT_{cc}$  and adding a fast tracking condensation temperature (here, the maximum capacity condensation temperature  $T_{cm}$ ) and adds the condensation temperature correction value  $KT_{cc}$  to the reference target condensation temperature  $KT_{cb}$  to thereby forcibly change the target condensation temperature  $T_{cs}$  to the maximum capacity condensation temperature  $T_{cm}$  (e.g., 46° C.) serving as the fast tracking condensation temperature. That is, the quick mode is a mode that does not allow the target condensation temperature  $T_{cs}$  to be changed to the highest condensation temperature  $T_{cex}$ . The changing of the condensation temperature correction value  $KT_{cc}$  in the fast changing mode (the powerful mode and the quick mode) and the control that corrects the target condensation temperature  $T_{cs}$  by adding the condensation temperature correction value  $KT_{cc}$  to the reference target condensation temperature  $KT_{cb}$  are also performed by the target refrigerant temperature changing part 84.

Then, after performing the processing of step ST15, the target refrigerant temperature changing part 84 returns to the processing of step ST12, and thereafter the processing of steps ST12, ST13, ST14, and ST15 is repeated.

Because of this fast changing mode, that is to say the fast changing control resulting from steps ST12, ST13, ST14, and ST15 during the heating operation, as shown in FIG. 8, the target condensation temperature  $T_{cs}$  is changed in such a way that the room temperatures  $T_r$  reach the set temperatures  $T_{rs}$  in a shorter amount of time compared to the case resulting from the slow changing mode (i.e., in the slow changing mode, the target condensation temperature  $T_{cs}$  is changed in such a way that the room temperatures  $T_r$  reach the set temperatures  $T_{rs}$  in a longer amount of time than in the fast changing mode). For this reason, by setting the mode to the fast changing mode, control trackability can be improved compared to a case where the mode is set to the slow changing mode. Because of this, here, by setting the mode to the target refrigerant temperature changing mode, priority can be given to energy conservation, and at the same time the degree of control trackability can be changed according to the preference of the user.

Furthermore, here, in cases other than a case where the temperature differences between the room temperatures  $T_r$  and the set temperatures  $T_{rs}$  exceed the threshold temperature difference (here, the predetermined temperature difference  $\Delta T_{rc2}$ ) and the number of indoor units in operation increases, the target condensation temperature  $T_{cs}$  is slowly changed by step ST13. For this reason, basically an excess of the air conditioning (heating) capacity of the outdoor unit 2 can be suppressed. Moreover, here, in a case where the temperature differences between the room temperatures  $T_r$  and the set temperatures  $T_{rs}$  exceed the threshold temperature difference (here, the predetermined temperature difference  $\Delta T_{rc2}$ ) and the number of indoor units in operation increases, that is to say a case where a large air conditioning (heating) capacity becomes necessary in the outdoor unit 2 as a result of the number of indoor units in operation increasing, as shown in FIG. 9, by performing fast changing control, the target con-

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densation temperature  $T_{cs}$  is changed to a fast tracking condensation temperature (here, the maximum capacity condensation temperature  $T_{cm}$  and the highest condensation temperature  $T_{cex}$ ). Because of this, here, by changing the target condensation temperature  $T_{cs}$ , energy conservation can be improved, and sufficient control trackability can be obtained even in a case where the number of indoor units in operation increases.

Furthermore, here, the reference target condensation temperature  $KT_{cb}$  is set in accordance with the outdoor temperature  $T_a$  by the automatic mode, so the target condensation temperature  $T_{cs}$  that is set as a result of a correction corresponding to the fast changing mode being made to the reference target condensation temperature  $KT_{cb}$  can further improve the degree of energy conservation.

Furthermore, here, the maximum value of the temperature differences between the room temperatures  $T_r$  and the set temperatures  $T_{rs}$  among the indoor units in operation (in an indoor thermostat ON state) is used as a condition for changing the target condensation temperature  $T_{cs}$ . For this reason, the target condensation temperature  $T_{cs}$  is changed in accordance with the indoor unit in which the largest air conditioning (heating) capacity is required. Because of this, here, the target condensation temperature  $T_{cs}$  can be promptly changed and control trackability can be improved.

Furthermore, here, the fast changing mode (fast changing control) can be set to either of two modes (control)—the powerful mode (powerful changing control) and the quick mode (quick changing control)—in which the degree of control trackability is further different. Additionally, when the mode is set to the powerful mode, the target condensation temperature  $T_{cs}$  is allowed to be changed to the highest condensation temperature  $T_{cex}$  exceeding the maximum capacity condensation temperature  $T_{cm}$ , so as shown in FIG. 9, control trackability is further improved compared to a case where the mode is set to the quick mode or a case where the mode is set to the target refrigerant temperature fixing mode. Because of this, here, by setting the mode to the fast changing mode, control trackability can be improved, and at the same time the degree of control trackability can be further changed according to the preference of the user.

(Economy Mode)

When the mode is set to the automatic mode and is set to the economy mode by the target refrigerant temperature mode setting part 83, during the cooling operation, in contrast to the fast changing mode and the slow changing mode described above, the reference target evaporation temperature  $KT_{eb}$  is set as the target evaporation temperature  $T_{es}$  without a correction being made to the reference target evaporation temperature  $KT_{eb}$  that was set in the automatic mode (i.e., only a change corresponding to the outdoor temperature  $T_a$  is made).

Furthermore, when the mode is set to the automatic mode and is set to the economy mode by the target refrigerant temperature mode setting part 83, during the heating operation, in contrast to the fast changing mode and the slow changing mode described above, the reference target condensation temperature  $KT_{cb}$  is set as the target condensation temperature  $T_{cs}$  without a correction being made to the reference target condensation temperature  $KT_{cb}$  that was set in the automatic mode (i.e., only a change corresponding to the outdoor temperature  $T_a$  is made).

In this way, when the mode is set to the automatic mode of the target refrigerant temperature changing mode, the mode can be set to any of three modes including, in addition to the fast changing mode and the slow changing mode, the economy mode in which the way of correcting the reference

target evaporation temperature  $K_{Teb}$  or the reference target condensation temperature  $K_{Tcb}$  that has been set in the automatic mode is different. Additionally, when the mode is set to the economy mode, the target evaporation temperature  $T_{es}$  or the target condensation temperature  $T_{cs}$  is set without a correction being made to the reference target evaporation temperature  $K_{Teb}$  or the reference target condensation temperature  $K_{Tcb}$ , so the degree of control trackability can be brought closest to the preference of the user. Because of this, here, by setting the mode to the automatic mode, the degree of energy conservation can be set, and at the same time the degree of control trackability can be changed according to the preference of the user.

#### —High-Sensitivity Mode—

In the high-sensitivity mode, in contrast to the automatic mode, the user sets the reference target evaporation temperature  $K_{Teb}$  or the reference target condensation temperature  $K_{Tcb}$ . Specifically, when the mode is set to the high-sensitivity mode by the target refrigerant temperature mode setting part **83**, the user can set the value of the reference target evaporation temperature  $K_{Teb}$  or the reference target condensation temperature  $K_{Tcb}$ . Here, the user can set the reference target evaporation temperature  $K_{Teb}$  by selecting any of several temperature values (e.g., 7, 8, 9, 10, and 11° C.) that are higher than the maximum capacity evaporation temperature  $T_{em}$ . Furthermore, the user can set the reference target condensation temperature  $K_{Tcb}$  by selecting any of several temperature values (e.g., 41 and 43° C.) that are lower than the maximum capacity condensation temperature  $T_{cm}$ .

Additionally, in the high-sensitivity mode, in contrast to the automatic mode, during the cooling operation or the heating operation, the user sets the reference target evaporation temperature  $K_{Teb}$  or the reference target condensation temperature  $K_{Tcb}$ , and the target refrigerant temperature changing part **84** changes the target evaporation temperature  $T_{es}$  or the target condensation temperature  $T_{cs}$  by further making a correction according to the same slow changing mode or the fast changing mode as in the automatic mode or by not making a correction (economy mode).

In this way, here, when the mode is set to the target refrigerant temperature changing mode by the target refrigerant temperature mode setting part **83**, the mode can be set to either of two modes—the automatic mode and the high-sensitivity mode—in which the way of setting the reference target evaporation temperature  $K_{Teb}$  or the reference target condensation temperature  $K_{Tcb}$  is different. Additionally, when the mode is set to the automatic mode, as described above, the reference target evaporation temperature  $K_{Teb}$  or the reference target condensation temperature  $K_{Tcb}$  is set in accordance with the outdoor temperature  $T_a$ , so the target evaporation temperature  $T_{es}$  or the target condensation temperature  $T_{cs}$  that is set as a result of a correction corresponding to the fast changing mode or the slow changing mode being made to the reference target evaporation temperature  $K_{Teb}$  or the reference target condensation temperature  $K_{Tcb}$  can further improve the degree of energy conservation compared to a case where the mode is set to the high-sensitivity mode. On the other hand, when the mode is set to the high-sensitivity mode, the degree of energy conservation can be set according to the preference of the user. Because of this, here, by setting the mode to the target refrigerant temperature changing mode, priority can be given to energy conservation, and at the same time the degree of energy conservation can be changed according to the preference of the user.

#### (Slow Changing Mode)

When the mode is set to the high-sensitivity mode and is set to the slow changing mode by the target refrigerant tempera-

ture mode setting part **83**, like in the case where the mode is set to the automatic mode, during the cooling operation, the evaporation temperature correction value  $K_{Tec}$  is changed as shown in steps ST1 to ST4 of FIG. 4. Additionally, the target evaporation temperature  $T_{es}$  is changed by making a correction that adds the evaporation temperature correction value  $K_{Tec}$  to the reference target evaporation temperature  $K_{Teb}$ .

Furthermore, when the mode is set to the high-sensitivity mode and is set to the slow changing mode by the target refrigerant temperature mode setting part **83**, like in the case where the mode is set to the automatic mode, during the heating operation also, the condensation temperature correction value  $K_{Tcc}$  is changed as shown in steps ST11 to ST14 of FIG. 5. Additionally, the target condensation temperature  $T_{cs}$  is changed by making a correction that adds the condensation temperature correction value  $K_{Tcc}$  to the reference target condensation temperature  $K_{Tcb}$ .

#### (Fast Changing Mode)

When the mode is set to the high-sensitivity mode and is set to the fast changing mode (the powerful mode or the quick mode) by the target refrigerant temperature mode setting part **83**, during the cooling operation, the same slow changing control resulting from steps ST1 to ST4 as in the slow changing mode described above is performed, and in a case where the temperature differences ( $T_r - T_{rs}$ ) have exceeded the threshold temperature difference and the number of indoor units in operation has increased, as shown in step ST5 of FIG. 4, fast changing control (powerful changing control or quick changing control) is performed in which the evaporation temperature correction value  $K_{Tec}$  and the target evaporation temperature  $T_{es}$  are forcibly changed to fast tracking evaporation temperatures (here, the maximum capacity evaporation temperature  $T_{em}$  and the lowest evaporation temperature  $T_{eex}$ ).

Furthermore, when the mode is set to the high-sensitivity mode and is set to the fast changing mode (the powerful mode or the quick mode) by the target refrigerant temperature mode setting part **83**, during the heating operation also, the same slow changing control resulting from steps ST11 to ST14 as in the slow changing mode described above is performed, and in a case where the temperature differences ( $T_{rs} - T_r$ ) have exceeded the threshold temperature difference and the number of indoor units in operation has increased, as shown in step ST15 of FIG. 5, fast changing control (powerful changing control or quick changing control) is performed in which the condensation temperature correction value  $K_{Tcc}$  and the target condensation temperature  $T_{cs}$  are forcibly changed to fast tracking condensation temperatures (here, the maximum capacity condensation temperature  $T_{cm}$  and the highest condensation temperature  $T_{cex}$ ).

#### (Economy Mode)

When the mode is set to the high-sensitivity mode and is set to the economy mode by the target refrigerant temperature mode setting part **83**, during the cooling operation, in contrast to the fast changing mode and the slow changing mode described above, the reference target evaporation temperature  $K_{Teb}$  is set as the target evaporation temperature  $T_{es}$  without a correction being made to the reference target evaporation temperature  $K_{Teb}$  that has been set in the high-sensitivity mode (i.e., in contrast to the automatic mode, without even a change corresponding to the outdoor temperature  $T_a$  being made).

Furthermore, when the mode is set to the high-sensitivity mode and is set to the economy mode by the target refrigerant temperature mode setting part **83**, during the heating operation, in contrast to the fast changing mode and the slow changing mode described above, the reference target conden-

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sation temperature  $KT_{cb}$  is set as the target condensation temperature  $T_{cs}$  without a correction being made to the reference target condensation temperature  $KT_{cb}$  that has been set in the high-sensitivity mode (i.e., in contrast to the automatic mode, without even a change corresponding to the outdoor temperature  $T_a$  being made).

In this way, when the mode is set to the high-sensitivity mode of the target refrigerant temperature changing mode, the mode can be set to any of three modes including, in addition to the fast changing mode and the slow changing mode, the economy mode in which the way of correcting the reference target evaporation temperature  $KT_{eb}$  or the reference target condensation temperature  $KT_{cb}$  that has been set in the high-sensitivity mode is different. Additionally, when the mode is set to the economy mode, the target evaporation temperature  $T_{es}$  or the target condensation temperature  $T_{cs}$  is set without a correction being made to the reference target evaporation temperature  $KT_{eb}$  or the reference target condensation temperature  $KT_{cb}$ , so the degree of control trackability can be brought closest to the preference of the user. Because of this, here, by setting the mode to the high-sensitivity mode, the degree of energy conservation can be set, and at the same time the degree of control trackability can be changed according to the preference of the user.

#### (4) Example Modification 1

In the embodiment described above, as shown in FIG. 4 and FIG. 5, the target refrigerant temperature changing part **84** determines, every first amount of waiting time  $t_1$ , whether or not the slow changing control (steps  $ST_3$ ,  $ST_4$ ,  $ST_{13}$ ,  $ST_{14}$ ) is necessary and also determines, every first amount of waiting time  $t_1$ , whether or not the fast changing control (steps  $ST_5$ ,  $ST_{15}$ ) is necessary. For this reason, both in a case where an increase in the number of indoor units in operation occurs and in a case where this is not so, the target refrigerant temperature changing part **84** can perform control only every first amount of waiting time  $t_1$ .

However, the fast changing control is performed in a case where the number of indoor units in operation increases, so it is preferable to ensure that the fast changing control can be promptly performed.

Therefore, here, as shown in FIG. 10 and FIG. 11, the target refrigerant temperature changing part **84** determines whether or not the slow changing control is necessary every time the first amount of waiting time  $t_1$  passes and determines whether or not the fast changing control is necessary every time a second amount of waiting time  $t_3$ , which is shorter than the first amount of waiting time  $t_1$ , passes.

For this reason, here, the fast changing control can be performed more frequently compared to the slow changing control, and the fact that the fast changing control has become necessary can be promptly detected.

Because of this, here, the control trackability of the fast changing control can be improved.

#### (5) Example Modification 2

In the embodiment described above and example modification 1, the reference target evaporation temperature  $KT_{eb}$  is set in accordance with the outdoor temperature  $T_a$  in the automatic mode and is set by the user in the high-sensitivity mode. Here, for example, in an operating state in which the outdoor temperature  $T_a$  is high and the room temperatures  $T_r$  are low, there can be cases where the humidity in the air conditioned spaces becomes higher than the relative humidity (usually about 60%) suitable for the room temperatures  $T_r$ .

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When the relative humidity becomes higher, discomfort increases in the air conditioned spaces, so this kind of operating state needs to be avoided.

Therefore, here, the reference target evaporation temperature  $KT_{eb}$  is restricted to be equal to or less than an upper limit evaporation temperature that has been set in accordance with the room temperatures  $T_r$ . For example, the upper limit evaporation temperature can be set on the basis of a function of the room temperatures  $T_r$ . Here, the relative humidity tends to become lower the higher the room temperatures  $T_r$  are, so the upper limit evaporation temperature is set on the basis of a function in which the upper limit evaporation temperature becomes higher as the room temperatures  $T_r$  become higher.

For this reason, here, the reference target evaporation temperature  $KT_{eb}$  that is set in the automatic mode and the high-sensitivity mode is restricted to be equal to or less than the upper limit evaporation temperature that has been set in accordance with the room temperatures  $T_r$ , so the humidity in the air conditioned spaces can be made equal to or less than the relative humidity suitable for the room temperatures  $T_r$ .

Because of this, here, discomfort in the air conditioned spaces can be suppressed, and at the same time the degree of energy conservation and the degree of control trackability can be changed according to the preference of the user.

#### (6) Example Modification 3

In the embodiment described above and example modifications 1 and 2, the target refrigerant temperature mode setting part **83** is disposed in the outdoor-side control unit **38**, but it is not limited to these. For example, although it is not illustrated in the drawings, in a case where the air conditioning apparatus **1** has a central control device such as a central remote controller that collectively controls the plural indoor units (and also plural outdoor units in a case where the air conditioning apparatus **1** has plural outdoor units), the target refrigerant temperature mode setting part **83** may be disposed in the central control device. In this case, it becomes possible to more easily perform the mode setting described above.

### INDUSTRIAL APPLICABILITY

The present invention is widely applicable to air conditioning apparatuses equipped with a refrigerant circuit configured as a result of plural indoor units being connected to an outdoor unit.

What is claimed is:

1. An air conditioning apparatus equipped with a refrigerant circuit configured with plural indoor units connected to an outdoor unit, the air conditioning apparatus comprising:

- a capacity controlling part controlling an air conditioning capacity of the outdoor unit such that an evaporation temperature of refrigerant in the refrigerant circuit becomes a target evaporation temperature; and
- a target refrigerant temperature mode setting part setting a target refrigerant temperature mode to one of
  - a target refrigerant temperature changing mode that changes the target evaporation temperature, and
  - a target refrigerant temperature fixing mode that fixes the target evaporation temperature,

- the target refrigerant temperature changing mode having a first changing mode that changes the target evaporation temperature in such a way that room temperatures of air conditioned spaces targeted by the indoor units reach set temperatures that are target values of the room temperatures in an amount of time, and

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a second changing mode that changes the target evaporation temperature in such a way that the room temperatures reach the set temperatures in a longer amount of time than in the first changing mode, and the first changing mode and the second changing mode being set by the target refrigerant temperature mode setting part.

2. The air conditioning apparatus according to claim 1, wherein

in the target refrigerant temperature fixing mode, the target evaporation temperature is fixed to a maximum capacity evaporation temperature corresponding to a case in which an air conditioning capacity of the outdoor unit is at 100% capacity.

3. The air conditioning apparatus according to claim 2, wherein

the first changing mode has

a first sub-mode that allows the target evaporation temperature to be changed to a lowest evaporation temperature exceeding the maximum capacity evaporation temperature and

a second sub-mode that does not allow the target evaporation temperature to be changed to the lowest evaporation temperature or the highest condensation temperature, and

the first sub-mode and the second sub-mode are set by the target refrigerant temperature mode setting part.

4. The air conditioning apparatus according to claim 1, wherein

the target refrigerant temperature changing mode further has

an automatic mode that sets a reference target evaporation temperature serving as a reference value of the target evaporation temperature in accordance with an outdoor temperature of an outside space where the outdoor unit is disposed and

a user-set mode in which a user sets the reference target evaporation temperature,

the first changing mode and the second changing mode are set, together with the automatic mode or the user-set mode, by the target refrigerant temperature mode setting part, and

the target evaporation temperature is changed by making, with respect to the reference target evaporation temperature, a correction corresponding to the first changing mode or the second changing mode.

5. The air conditioning apparatus according to claim 4, wherein

the target refrigerant temperature changing mode further has an economy mode in which the reference target evaporation temperature that has been set in the automatic mode or the user-set mode is set as the target evaporation temperature without a correction being made to the reference target evaporation temperature, and

the economy mode is set, together with the automatic mode or the user-set mode, by the target refrigerant temperature mode setting part.

6. The air conditioning apparatus according to claim 4, wherein

the reference target evaporation temperature is restricted to be no more than an upper limit evaporation temperature that has been set in accordance with the room temperatures.

7. The air conditioning apparatus according to claim 2, wherein

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the target refrigerant temperature changing mode further has

an automatic mode that sets a reference target evaporation temperature serving as a reference value of the target evaporation temperature in accordance with an outdoor temperature of an outside space where the outdoor unit is disposed and

a user-set mode in which a user sets the reference target evaporation temperature,

the first changing mode and the second changing mode are set, together with the automatic mode or the user-set mode, by the target refrigerant temperature mode setting part, and

the target evaporation temperature is changed by making, with respect to the reference target evaporation temperature, a correction corresponding to the first changing mode or the second changing mode.

8. The air conditioning apparatus according to claim 7, wherein

the target refrigerant temperature changing mode further has an economy mode in which the reference target evaporation temperature that has been set in the automatic mode or the user-set mode is set as the target evaporation temperature without a correction being made to the reference target evaporation temperature, and

the economy mode is set, together with the automatic mode or the user-set mode, by the target refrigerant temperature mode setting part.

9. The air conditioning apparatus according to claim 7, wherein

the reference target evaporation temperature is restricted to be no more than an upper limit evaporation temperature that has been set in accordance with the room temperatures.

10. The air conditioning apparatus according to claim 3, wherein

the target refrigerant temperature changing mode further has

an automatic mode that sets a reference target evaporation temperature serving as a reference value of the target evaporation temperature in accordance with an outdoor temperature of an outside space where the outdoor unit is disposed and

a user-set mode in which a user sets the reference target evaporation temperature,

the first changing mode and the second changing mode are set, together with the automatic mode or the user-set mode, by the target refrigerant temperature mode setting part, and

the target evaporation temperature is changed by making, with respect to the reference target evaporation temperature, a correction corresponding to the first changing mode or the second changing mode.

11. The air conditioning apparatus according to claim 10, wherein

the target refrigerant temperature changing mode further has an economy mode in which the reference target evaporation temperature that has been set in the automatic mode or the user-set mode is set as the target evaporation temperature without a correction being made to the reference target evaporation temperature, and

the economy mode is set, together with the automatic mode or the user-set mode, by the target refrigerant temperature mode setting part.

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12. The air conditioning apparatus according to claim 10, wherein

the reference target evaporation temperature is restricted to be no more than an upper limit evaporation temperature that has been set in accordance with the room temperatures.

13. An air conditioning apparatus equipped with a refrigerant circuit configured with plural indoor units connected to an outdoor unit, the air conditioning apparatus comprising:

a capacity controlling part controlling an air conditioning capacity of the outdoor unit such that a condensation temperature of refrigerant in the refrigerant circuit becomes a target condensation temperature; and

a target refrigerant temperature mode setting part setting a target refrigerant temperature mode to one of a target refrigerant temperature changing mode that changes the target condensation temperature, and a target refrigerant temperature fixing mode that fixes the target condensation temperature,

the target refrigerant temperature changing mode having a first changing mode that changes the target condensation temperature in such a way that room temperatures of air conditioned spaces targeted by the indoor units reach set temperatures that are target values of the room temperatures in an amount of time, and

a second changing mode that changes the target condensation temperature in such a way that the room temperatures reach the set temperatures in a longer amount of time than in the first changing mode, and the first changing mode and the second changing mode being set by the target refrigerant temperature mode setting part.

14. The air conditioning apparatus according to claim 13, wherein

in the target refrigerant temperature fixing mode, the target condensation temperature is fixed to a maximum capacity condensation temperature corresponding to a case in which an air conditioning capacity of the outdoor unit is at 100% capacity.

15. The air conditioning apparatus according to claim 14, wherein

the first changing mode has

a first sub-mode that allows the target condensation temperature to be changed to a highest condensation temperature exceeding the maximum capacity condensation temperature and

a second sub-mode that does not allow the target condensation temperature to be changed to the highest condensation temperature, and

the first sub-mode and the second sub-mode are set by the target refrigerant temperature mode setting part.

16. The air conditioning apparatus according to claim 13, wherein

the target refrigerant temperature changing mode further has

an automatic mode that sets a reference target condensation temperature serving as a reference value of the target condensation temperature in accordance with an outdoor temperature of an outside space where the outdoor unit is disposed and

a user-set mode in which a user sets the reference target condensation temperature,

the first changing mode and the second changing mode are set, together with the automatic mode or the user-set mode, by the target refrigerant temperature mode setting part, and

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the target condensation temperature is changed by making, with respect to the reference target condensation temperature, a correction corresponding to the first changing mode or the second changing mode.

17. The air conditioning apparatus according to claim 16, wherein

the target refrigerant temperature changing mode further has an economy mode in which the reference target condensation temperature that has been set in the automatic mode or the user-set mode is set as the target condensation temperature without a correction being made to the reference target condensation temperature, and

the economy mode is set, together with the automatic mode or the user-set mode, by the target refrigerant temperature mode setting part.

18. The air conditioning apparatus according to claim 14, wherein

the target refrigerant temperature changing mode further has

an automatic mode that sets a reference target condensation temperature serving as a reference value of the target condensation temperature in accordance with an outdoor temperature of an outside space where the outdoor unit is disposed and

a user-set mode in which a user sets the reference target condensation temperature,

the first changing mode and the second changing mode are set, together with the automatic mode or the user-set mode, by the target refrigerant temperature mode setting part, and

the target condensation temperature is changed by making, with respect to the reference target condensation temperature, a correction corresponding to the first changing mode or the second changing mode.

19. The air conditioning apparatus according to claim 18, wherein

the target refrigerant temperature changing mode further has an economy mode in which the reference target condensation temperature that has been set in the automatic mode or the user-set mode is set as the target condensation temperature without a correction being made to the reference target condensation temperature, and

the economy mode is set, together with the automatic mode or the user-set mode, by the target refrigerant temperature mode setting part.

20. The air conditioning apparatus according to claim 15, wherein

the target refrigerant temperature changing mode further has

an automatic mode that sets a reference target condensation temperature serving as a reference value of the target condensation temperature in accordance with an outdoor temperature of an outside space where the outdoor unit is disposed and

a user-set mode in which a user sets the reference target condensation temperature,

the first changing mode and the second changing mode are set, together with the automatic mode or the user-set mode, by the target refrigerant temperature mode setting part, and

the target condensation temperature is changed by making, with respect to the reference target condensation temperature, a correction corresponding to the first changing mode or the second changing mode.

21. The air conditioning apparatus according to claim 20,  
wherein

the target refrigerant temperature changing mode further  
has an economy mode in which the reference target  
condensation temperature that has been set in the auto- 5  
matic mode or the user-set mode is set as the target  
condensation temperature without a correction being  
made to the reference target condensation temperature,  
and

the economy mode is set, together with the automatic mode 10  
or the user-set mode, by the target refrigerant tempera-  
ture mode setting part.

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